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,	REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
(14)	HDL-TR-1959	2. BOYT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
6	Bipolar Transistor and Diode Electrical Transients Predic Modeling versus Experimental Testing 1. Junction Capacit	ctive Failure	Technical Report.	
(9)	Damage Model, 7. Author Michael J./Vrabel	·	B. CONTRACT OR GRANT NUMBER(a)	
	PERFORMING CASANTEATION HAME AND ADDRESS Harry Diamond Laboratories 2800 Powder Mill Road Adelphi, MD 20783		Program Ele: 6.21.20.A	
į	US Army Materiel Development Readiness Command Alexandria, VA 22333	<u> </u>	Juny 81 13. NUMBER UF PAGE 100 (2) 99	
	14. MONITORING AGENCY NAME & ADDRESS(II dilleren	t from Controlling Office)	UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
· ·	16. DISTRIBUTION STATEMENT (of this Report)			

Approved for public release; distribution unlimited.

17. DISTRIBUTION STATEMENT (of the ebetract entered in Block 20, If different from Report)

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18. SUPPLEMENTARY NOTES

DRCMS Code: 612120.H.250011
DA Project: 1L162120AH25
HDL Project: X750E2

15. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Semiconductor damage Semiconductor transient failure Junction capacitance damage model

Electromagnetic pulse

20. AND AACT (Continue on reverse ship if necessary and identify by block sumber)

For all the difficulties engendered in its use, semi-conductor device damage data are an integral part of many programs of electromagnetic pulse vulnerability assessment and hardening. Experimental damage data, which are generated only as a result of dedicated efforts, can be expected to be available for only a minor fraction of all semiconductor devices. This limited supply has spurred efforts to develop

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predictive damage models, in order to bypass the tedious experimental requirements for generating damage data. The predictive ability of the best of these models, the junction capacitance damage model, is investigated in detail.

Central to this study is a library of experimental damage data for 46 silicon device types, comprising bipolar transistors and diodes tested at the 10-, 1-, and 0.17µs pulse durations. These are devices from the front ends of a number of Army systems and represent radio, field wire, and cable functions with operating ranges in the direct current (dc) to microwave region. Of the 46 experimental devices comprising 68 junction types (collector-to-base and emitter-to-base junctions treated as distinct for all transistors), sufficient published manufacturers' data were available for the damage modeling of 11 junctions. These were supplemented with measured parameters for 27 junction types. No measurable difference was observed between the model's predictive capability by using the experimental parameters and that by using manufacturers' model parameters. The ratios of experimental power to damage (for all tested pulse durations) to predicted value span a range from 0.00077 to 18--a skewed distribution, with 59 percent of all predicted values being overestimates of the power to damage.

With only 16 percent of the test-device population having published parameters to allow the junction capacitance damage model to be used, it is a valuable exercise to develop alternative, simpler damage models -- not so much as a substitute for the junction capacitance model, but rather as a standard for comparison. The first considered was the dc power It was bas on the supposition that there is rating model. some correlation between dc power ratings and transient power to No distinction was made in the development of this model between forward or reverse dc ratings. The resultant model was applicable to 88 percent of the test-device population (based on published parameters) and demonstrated an agreement power-to-damage with experimental data that approximately two to four times poorer than the junction capacitance model. A second model was developed based on the manufacturers' rating of devices as high power or low power. This model considered the entire population of bipolar diodes (excluding microwave devices) transistors and equatable to either of two devices with damage constants of 0.089 and 6.1 W-s $^{1/2}$. This model was applicable to 90 percent of the test population and demonstrated the same level of correlation with the experimental damage data as did the junction capacitance damage model.

A comparison of the predictive capability of the junction capacitance damage model with the scatter in the experimental damage data indicates that the use of the failure model requires an order of magnitude larger conservatism in the lower bounding of device failure than the use of an experimentally established damage curve.

CONTENTS

	<u>P</u> (age
1.	INTRODUCTION	5
2.	EXAMINATION	5
3.	RESULTS	7
4.	SUMMARY AND FINAL ANALYSIS	22
DIS	TRIBUTION	95
APP	ENDIX ADAMAGE MODELING COMPUTER CODE	25
	FIGURES	
1	Histogram of N from damage equation $P_D = Kt^{-N}$	9
2	Histogram of experimental power to damage for pulse duration of 0.1 µs	11
3	Histogram of experimental power to damage for pulse duration of 1 µs	11
4	Histogram of experimental power to damage for pulse duration of 10 µs	12
5	Histogram of maximum deviation of device damage from experimentally established damage curve	12
6	Superimposed histograms of ratio of experimental power to damage to predicted value based on junction capacitance damage model	14
7	Confidence level for junction capacitance damage model test of standard population	15
8	Confidence level for junction capacitance damage model test of composite standard population	16
9	Confidence level for dc power rating model	20
10	Confidence level for power class damage model	22
	TABLES	
1	Junction Capacitance Damage Model	13
2	Constants A_1 , A_2 , and A_3 for Direct Current Power Rating Model $P_D/P_{DC} = A_1t^{-1} + A_2t^{-1/2} + A_3$	19
3	Damage Constants for High and Low Power Devices for Power Class	

1. INTRODUCTION

Component transient damage data are an integral part of any comprehensive program of electromagnetic pulse (EMP) vulnerability assessment and hardening. In general, semiconductor devices represent the most vulnerable of components and are the devices that have received the most intensive study. With approximately 75,000 bipolar transistor and diode types alone (of which approximately 2000 have military specifications), experimental damage data, data available only as a result of dedicated efforts, can be expected to be available for only a minor fraction of semiconductor devices. This limitation has spurred efforts to bypass the tedious experimental requirements to generate damage data by developing predictive damage models. Three semiempirical damage models are presently in general use. 1 These are designed to predict the failure level of bipolar transistors and diodes under conditions of reverse bias. There is amassed in the literature much information on the predictive ability of these models, much of it sketchy with no well defined standards for drawing a comparison and some of it contradictory. Based on the most exhaustive of 'hese studies, there appears no clearly superior model.²

The purpose of this study is to focus on one of these, the junction capacitance damage model, and to attempt to establish some standards whereby the user can judge its adequacy. Central to this examination is a library of experimental damage data for 59 device types generated for the Army's former Multiple Systems Evaluation Program. These represent transistors and diodes incorporated into the front ends of a number of tactical single and multichannel radios, associated with circuits operating from the direct current (dc) to the microwave region. These data are taken from the unpublished work of Bruno Kalab of the Harry Diamond Laboratories.

This study is a narrowly defined investigation of the predictive ability of the junction capacitance damage model. It must always be borne in mind that, when the adequacy of the model is judged, it must be considered within the context of all sources of error in a program of EMP vulnerability assessment and hardening. Since model accuracy is a subjective quantity to be measured by the particular needs of the user, no conclusions are to be drawn. Rather, a set of standards is to be developed whereby the effectiveness of the model for particular applications can be judged.

¹DNA EMP (Electromagnetic Pulse) Handbook (U), Defense Nuclear Agency DNA 2114H (July 1979). (CONFIDENTIAL)

²D. R. Alexander, G. L. Brown, and J. B. Almassy, Electromagnetic Susceptibility of Semiconductor Components, Air Force Weapons Laboratory AFWL-TR-74-280 (September 1975).

2. EXAMINATION

Most predictive failure models for semiconductors are based on the work by Wunsch and Bell. 3 Based on a thermal model for failure, Wunsch and Bell developed the expression

$$P_D = \kappa e^{-N} \quad , \tag{1}$$

where P_D is the power to failure for a square pulse, K is a constant characteristic of the device (damage constant), t is the duration of the power pulse, and, for the Wunsch-Bell form of equation (1), N = 0.5. This value for N is treated as valid for junction reverse bias in at least the 0.1— to 10-µs range. It was observed that there existed a measure of correlation between power to damage and P-N junction area. From this observation were developed three analytical models for predicting device failure (under reverse bias) based on manufacturers' specifications. The first two are called thermal resistance models and are based on a simple resistance-capacitance (R-C) network for which heat flow from the junction area is treated as an analog of current, and temperature drop is treated as an analog of electric potential.

The thermal resistance models (incorporated into the Wunsch-Bell equation) are

$$P_D = A_1 \theta_{JC}^{-B_1} t^{-0.5}$$
 (2)

$$P_{D} = A_{2} \theta_{JA}^{-B_{2}} t^{-0.5} , \qquad (3)$$

where A_1 , A_2 , B_1 , and B_2 are experimentally determined constants and

$$\theta_{JC} = \frac{T_{J(MAX)} - T_{C}}{P_{D}} , \qquad (4)$$

³D. C. Wunsch and R. R. Bell, Determination of Threshold Failure Levels of Semiconductor Diodes and Transistors due to Pulse Voltages, IEEE Trans. Nucl. Sci., NS-15 (December 1968), 244-259.

⁴D. C. Wunsch, R. L. Cline, and G. R. Case, Semiconductor Vulnerability, Phase II Report, Theoretical Estimates of Failure Levels of Selected Semiconductor Diodes and Transistors, Braddock, Dunn and McDonald, Inc., Albuquerque, NM, BDM/A-42-69-R (August 1970).

$$\theta_{\rm JA} = \frac{{\rm T}_{\rm J}(\rm MAX)}{{\rm P}_{\rm D}} , \qquad (5)$$

where $T_{J(MAX)}$ is the maximum operating junction temperature and P_D is the total power dissipation at case temperature T_C or ambient temperature T_{AMB}

The junction capacitance model is based on the relationship between junction area and capacitance. The form of this model (incorporated into the Wunsch-Bell equation) is

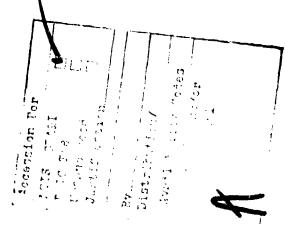
$$P_{E_i} = A_3 C_j V_{BD}^{B3} t^{-0.5} , \qquad (6)$$

where ${\bf A_3}$ and ${\bf B_3}$ are experimentally established constants, ${\bf C_j}$ is junction capacitance, and ${\bf V_{BD}}$ is junction breakdown voltage.

To reasonably test model predictions, a representative sample of experimental data is essential. The term "representative" is used advisedly since a small sample taken from a large population must be chosen carefully. All devices are taken from the front ends of an array of Army communications systems. These interface circuits represent radio, field wire, and coaxial cable functions. No devices were prescreened. Instead, all devices were selected on the basis of their proximity to the EMP coupling source with no exclusion on the basis of potential power handling capability, and all devices were chosen without regard to previously published device data. This latter condition insured that all devices were tested employing the same methodology and the same standards. All devices were obtained from federal stocks over a number of years without regard to manufacturer, device lot, or supplier. To the extent that such a selection process defines a general device population selected from among the types of devices of most interest in a transient damage analysis, then the test population can be called representative.

3. RESULTS

This device population (to be referred to as the standard population) was employed in this study:



Silicon devices

2N 32 6A (C-B)	1N752A
2N328A(E-B)	PC 115
2N335(C-B)	1N3026B: JAN
2N335(E-B)	1N3611
2N336: JAN(C-B)	1N 3995A
2N336: JAN (E-B)	1N3016B
2N2484 (C-B)	1N414;
2N2484(E~B)	10D2
2N3736(C−B)	2N2857(C-B)
2N3736(E-B)	2N2857(E-B)
2N930 (C-B)	2N3375(C-B)
2N930 (≅-B)	2N3375(E-B)
2N2481 (C-B)	2N1490: JAN(C-B)
2N2481 (E-B)	2N1490: JAN(E-B)
2N2907A(C-B)	2N3584(C-B)
2N2907A(E-B)	2N3584(E-B)
2N2222A(C-B)	2N2894(C-B)
2N2222A(E-B)	2N2894(E-B)
1N4384	2N5829(C-B)
rs911-3465	2N5929(E-B)
1ท816	2N3013: JAN(C-B)
1N21WE	2N3013: JAN(E-B)
1n914a	CA3018(C-B)

CA3018(E-B)
SMB52617(C-B)
SMB52617(E-B)
2N1613: JAN(C-B)
2N1613: JAN(E-B)
2N 1485: JAN (C-B)
2N1485: JAN(E-B)
2N3439(C-B)
2N3439(E-B)
2N706: JAN(C-B)
2N706: JAN(E-B)
1R-69-6735
1N2580
1N571A: JAN
1N 485B: JAN
1N2991B: JAN
1N 30 5B: JAN
MO1054
1N 7 46A: JAN
1N645: JAN
1N1202RA: JAN
1N1731A: JAN

Germanium devices

2N 40 4A (C-B)	2N396A(E-B)	2N705: JAN (E-B)
2N404A(E-B)	2N428M: JAN(C-E)	2N465M: JAN(C-B)
2N297A (C-B)	2N 428M: JAN (E-B)	2N466M: JAN(E-B)
2N297A(E-B)	2N393: JAN(C-B)	2N 1042RA: JAN (C-B)
2N526(C-B)	2N393: JAN(E-B)	2N1042RA: JAN (E-B)
2N526(E-B)	2N501A: JAN(C-B)	1N277: JAN
1N270	2N501A: JAN(E-B)	MS1040
2N396A(C-B)	2N705: JAN(C-B)	

Separate collector-to-base (C-B) and emitter-to-base (E-B) damage characteristics for all transistors yield 91 P-N junction types. Power-to-failure curves are available for these devices in the 0.1- to $10-\mu s$

range, with some exceptions. If, for the devices with damage data in the aforementioned range, a fit is made to equation (1), the histogram for N given in figure 1 results.

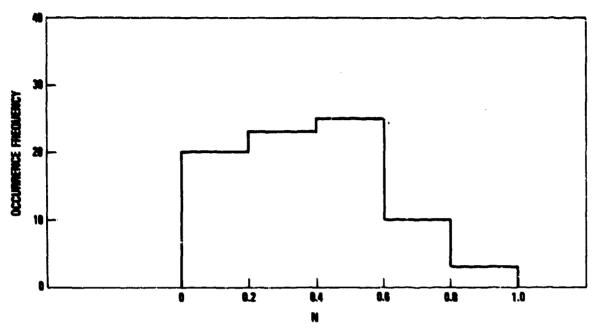


Figure 1. Histogram of N from damage equation $P_D = Rt^{-N}$ for standard population fitted in 0.1- to 10-µs range.

It will prove important for this study to consider the spread in the standard population power to damage and to have damage values for all tested devices. Because of test equipment limitations, some of the devices were undamageable, particularly for the shortest pulses. All testing was performed about the 0.1-, 1-, and 10- μ s pulse durations. For devices with data missing at the 0.1- μ s pulse duration, it becomes a simple matter to extrapolate from the 1- and 10- μ s data. An examination of all data revealed that extrapolation could be done with a high level of confidence; as a consequence, no distinction is made between these extrapolated data and measured data. For devices with data missing at the 0.1- and 1- μ s pulse durations, extrapolation becomes much less accurate. By relying on equation (1), data at 10 μ s can be used to extrapolate to 0.1 and 1 μ s:

$$\frac{P_{D}(1 \text{ } \mu s)}{P_{D}(10 \text{ } \mu s)} = \left(\frac{1}{10}\right)^{-N} \quad \text{and} \quad \frac{P_{D}(0.1 \text{ } \mu s)}{P_{D}(10 \text{ } \mu s)} = \left(\frac{1}{100}\right)^{-N} \quad . \tag{7}$$

Figure 1 indicates a value anywhere The choice of N is critical. between 0 and 1. If N = 0.5 is chosen, then this results in a maximum error at the 1-µs rulse duration of a factor of 3.16 and at the 10-µs pulse duration of a factor of 10. For some devices, the maximum nodamage pulse power is used to improve upon these potential error factors in the choice of extrapolated damage levels. The final situation is no power-to-damage data for any pulse duration. This occurred with a single device (100995A). For this device, the junction capacitance model was used to predict damage. The predicted value is compatible with the maximum no-damage power pulse. This compatibility represents the unusual situation of using a model to contribute to a distribution that is part of a test of the model. The predicted value was included since it was considered more important to achieve a complete set of data for the standard device distribution than to be concerned with a single anomalous point. Beyond this distribution, little further use is made of the 1N3995A damage data. The resultant distributions for the standard device population are given in figures 2 through 4. The powerto-damage values for the individual devices are given in appendix A. Sources of uncertainty in the experimental damage data can be classified as these:

- a. The natural variability in the levels to failure in any population used to define a damage curve
- b. The deviation in the makeup of the test population from that which is representative of a population of interest to the user

There is no way that a study can come to terms with the latter source of uncertainty, except to anticipate the interest of the greatest number of users and to select a population accordingly. The former source can be described by using standard error theory. In anticipation of a more detailed description of the level of variability in the test population later in the report, figure 5 presents as a histogram the range in the data defined as

V'/V , for V' > V

or

V/V', for V > V'

where V' is the experimental damage data point with the largest deviation from the damage curve and V is the corresponding value from the damage curve. These are values for all device types of the standard test population under reverse bias. Figure 5 represents the maximum deviation from the experimentally defined damage curve for a typical population of 9 to 15 tested components.

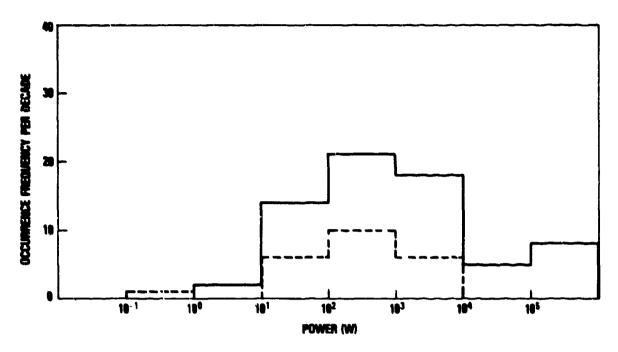


Figure 2. Histogram of experimental power to damage for pulse duration of 0.1 μ s for silicon devices of standard population (solid curve) with superimposed curve for germanium devices (dashed curve).

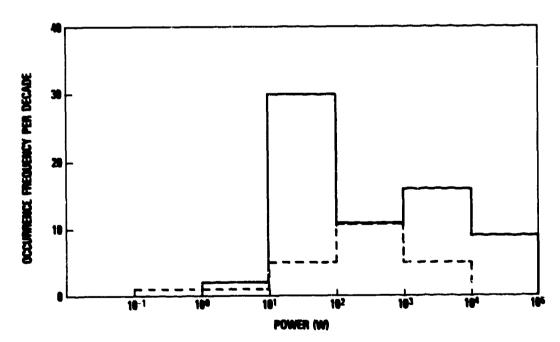


Figure 3. Histogram of experimental power to damage for pulse duration of 1 μ s for silicon devices of standard population (solid curve) with superimposed curve for germanium devices (dashed curve).

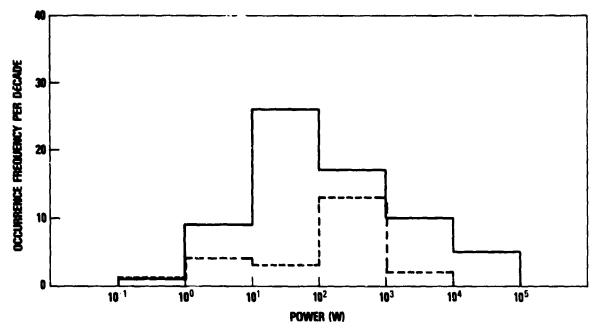


Figure 4. Histogram of experimental power to damage for pulse duration of 10 μ s for silicon devices of standard population (solid curve) with superimposed curve for germanium devices (dashed curve).

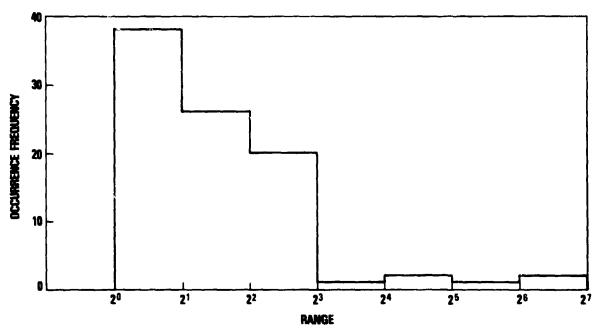


Figure 5. Histogram of maximum deviation of device damage from experimentally established damage curve for all devices of standard population defined as ratio with corresponding point on damage curve.

The most recent form of the junction capacitance damage model, including the experimentally established constants, is given in table 1. A number of difficulties are encountered in applying this model to the standard device population. The model is not applicable to germanium devices. For all silicon transistors, a knowledge of device construction is required--a quantity that is sometimes difficult to Similarly, junction capacitance and obtain from the literature. breakdown voltage are often unobtainable. For transistors, these parameters are rarely available for the base-to-emitter junction. consequence is that the model, based on published device parameters, is applicable to only 12 percent of the standard device population. If germanium devices are excluded from the standard population, this figure increases to 16 percent. To supplement missing data, experimentally established parameters for junction capacitance and breakdown voltage were employed. These increased the size of the silicon standard population to which the model was applicable to 47 percent.

TABLE 1. JUNCTION CAPACITANCE DAMAGE MODEL

Devices	$K = Pt^{1/2}$	
Diodes and nonplanar silicon transistors	$\kappa = 4.97 \times 10^{-3} \text{C}_{J} \text{V}_{BD}^{0.57}$	
Mesa and planar silicon transistors	$K = 1.66 \times 10^{-4} \text{C}_{J} \text{V}_{BD}^{0.992}$	

Note: For transistors, $C_J = C_{ob}$ and $V_{BD} = BV_{cbo}$.

Source: DNA EMP (Electromagnetic Pulse)
Handbook (U), Defense Nuclear Agency DNA 2114H
(July 1979). (CONFIDENTIAL)

It has been reported in the literature that little improvement in the predictive capability of this junction capacitance damage model occurs when experimental input parameters are substituted for published values.² This study supports that conclusion. To compare the predictive capability of the model using experimental and published parameters, the data are presented in two formats. The quantities presented are not the predicted values, but rather the scatter in the

²D. R. Alexander, G. L. Brown, and J. B. Almassy, Electromagnetic Susceptibility of Semiconductor Components, Air Force Weapons Laboratory AFWL-TR-74-280 (September 1975).

predicted values defined as the ratio of the experimental power to damage to the predicted value. These data are presented as a histogram of the population distribution in figure 6. They are presented also as a function of the percentage confidence level. The percentage confidence level is defined as the percent of the subject population with a scatter less than or equal to the given value. For this mode of presentation, the scatter is given as the spread in the data without regard to whether the predicted value is greater or less than the experimental value. This means that for values of the predicted-toexperimental ratio for damage less than 1, the data presented are the inverse of this ratio. This mode of presentation provides a convenient way to judge the utility of the model based on the varying degrees of confidence required by the diversity of potential model users. corresponding curves for the experimental and published model parameters are given in figure 7.

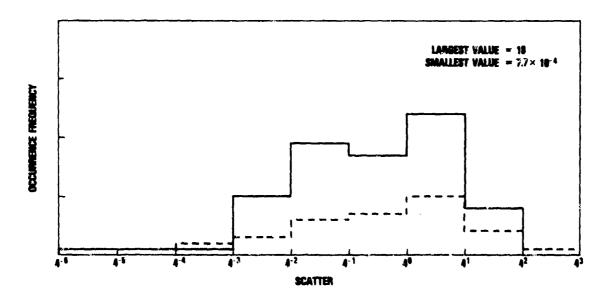


Figure 6. Superimposed histograms of ratio of experimental power to damage to predicted value based on junction capacitance damage model: experimental parameters for junction capacitance and breakdown voltage (solid curve) and manufacturers' parameters (dashed curve).

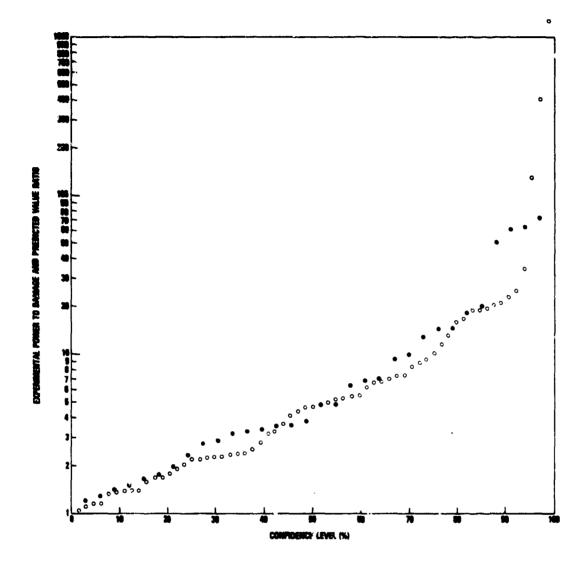


Figure 7. Confidence level for junction capacitance damage model test of standard population: published parameters (solid circles) and experimental values for junction capacitance and breakdown voltage (open circles); all extrapolated values for experimental damage data are excluded from standard population.

All further reference to the predictions of the junction capacitance damage model is to a composite of data corresponding to the model predictions based on experimental parameters plus those several devices not included in this lot for which sufficient published parameters were available. The device population can be ascertained from the data

presented in appendix A. This composite curve is presented in figure 8 for the standard population both including and excluding the extrapolated experimental damage values.

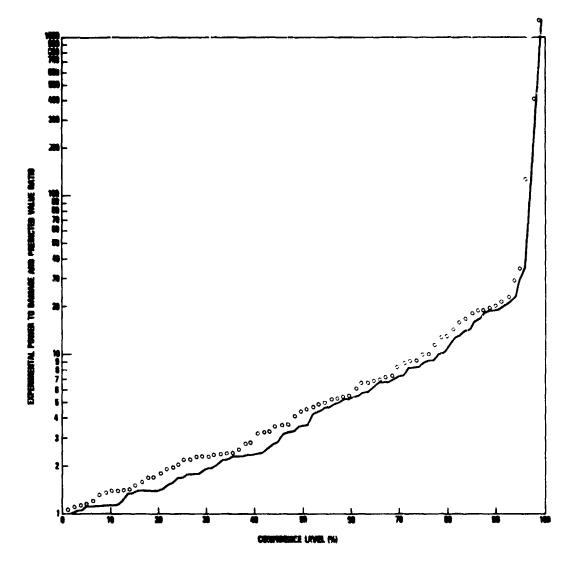


Figure 8. Confidence level for junction capacitance damage model test of composite standard population: all extrapolated values for experimental damage data are excluded from standard population (circles) and extrapolated values are included (solid curve).

Much of the convenience of the junction capacitance model is lost because of the limited availability of the requisite published It is an informative exercise to test the performance of the junction capacitance model by constructing alternative, simpler damage models. The basis for the junction capacitance damage model was the observation that there appeared to be a correlation between junction area and transient power level to damage. It is not an unreasonable supposition to theorize some measure of correlation between device do power rating and transient power level to failure. This model is to be referred to as the dc power rating model. Since this model is being proposed not so much as a potentially more accurate substitute, but rather as a standard for comparing the junction capacitance model, rigor is sacrificed for convenience of use and general applicability. Since devices such as rectifiers have power ratings for forward bias and devices such as reference diodes have power ratings for reverse bias, no distinction is to be made between forward or reverse bias in developing the model. For diodes without power ratings, but with a maximum rated current, a power rating is derived by selecting a reasonable corresponding junction potential. Similarly, power ratings for transistors are assumed to apply to the C-B and the E-B junctions. By these standards, sufficient published data are available to apply such a model to 88 percent of the standard silicon device population.

To develop and test the dc power rating model, the standard silicon device population is divided into two groups. Population A (containing approximately half the devices) is that segment lacking sufficient information to apply the junction capacitance damage model, but for which dc power ratings (as previously defined) exist. Population B is the same as population A, but contains those devices to which the junction capacitance damage model is applicable. By using population A to develop the dc power rating model and population B to test its predictive capability, a good comparison of the alternative damage models becomes possible. Since experimental data for constructing the model are available about the 0.1-, 1-, and 10-µs pulse durations, a particularly simple model to fit these data is of the form

$$P_D/P_{DC} = A_1 t^{-1} + A_2 t^{-1/2} + A_3$$
 (8)

where P_D is the average power to damage for population A devices at pulse duration t and P_{DC} is the corresponding average dc power rating. Although an equation of the form of equation (8) can be readily fitted to the device data, care must be used in extrapolating this relationship beyond the pulse durations used for the fit. For data at 0.1, 1, and 10 μ s, constants A_1 , A_2 , and A_3 become (t in units of s)

$$A_1 = 5.1 \times 10^{-7} \frac{P_D(10 \ \mu s)}{P_{DC}} - 6.7 \times 10^{-7} \frac{P_D(1 \ \mu s)}{P_{DC}}$$
 (9)

$$+ 1.6 \times 10^{-7} \frac{P_D(0.1 \mu s)}{P_{DC}}$$
,

$$A_{2} = -2.1 \times 10^{-3} \frac{P_{D}(10 \ \mu s)}{P_{DC}} + 2.3 \times 10^{-3} \frac{P_{D}(1 \ \mu s)}{P_{DC}}$$

$$-2.1 \times 10^{-4} \frac{P_{D}(0.1 \ \mu s)}{P_{DC}} , \qquad (10)$$

$$A_3 = 1.6 \frac{P_D(10 \ \mu s)}{P_{DC}} - 0.68 \frac{P_D(1 \ \mu s)}{P_{DC}} + 0.052 \frac{P_D(0.1 \ \mu s)}{P_{DC}} . \tag{11}$$

The choice of the ratios of $P_{\rm D}/P_{\rm DC}$ is based on the nature of the experimental device population. To choose as the ratios of $P_{\rm D}/P_{\rm DC}$ the average of the selected population requires careful consideration of the definition to be applied to average. The device experimental damage data population is not a normal distribution, and included within this distribution are a number of devices with extrapolated powers to damage. If the average value for $P_{\mathrm{D}}/P_{\mathrm{DC}}$ is taken as the arithmetic mean of the distribution, then the error inherent in the extrapolated values, values clustered at the high power end of the distribution, poses the possibility of an average value unrepresentative of the actual population. If the average value is taken as the median value of the distribution, then the uncertainty of the extrapolated values (if their number count is not too large) is eliminated, but at the risk that the median is not the value most representative of the population. Because of these uncertainties, both the arithmetic mean and the median are to be used for all modeling. The values developed to these standards for A_1 , A_2 , and A_3 for population A are given in table 2. The junction capacitance damage model and the dc power rating model applied to population B are compared in figure 9.

The correlation to be drawn between these curves is a function of the confidence level desired in the predictions. It is clearly beyond the scope of this study, being based on a limited data base, to approach the 100-percent level. Although all curves are extended to values approaching 100 percent, this extension is based on very few data

points. The consequence is that caution must be exercised in interpreting into the high confidence region. In the 50- to 90-percent confidence range, the dc power rating model yields a correlation with the experimental power to damage two to four times poorer than the junction capacitance damage model.

TABLE 2. CONSTANTS A_1 , A_2 , AND A_3 FOR DIRECT CURRENT POWER RATING MODEL $P_D/P_{DC} = A_1 t^{-1} + A_2 t^{-1/2} + A_3$

Statistic	A	A ₂	A 3
	(W-s)	(W-s- ^{/2})	(W)
Arithmetic mean	5.58 × 10 ⁻⁴	0.309	34.2
Median	9.87 × 10 ⁻⁶	0.101	22.7

An examination of the spread in the junction capacitance damage model predictions and the spread in the damage data of figures 2 to 4 indicates that it should be possible to define two power levels that cover the range of experimental damage data with a spread comparable to that of the junction capacitance model. As an attempt at such a model, which is called the power class model, all devices are classified as either high or low power devices based on published data.* Transistors are routinely classified as either high or low power—the dividing line, with some exceptions, is a power rating of 1 W. If the same 1-W standard is applied to diodes, then the semiconductor population can be divided into two classes. For model development for those diodes without a power rating, all rectifiers, silicon reference diodes, and varistors are considered high power, and the remaining devices are considered low power. This division results in a model applicable to 90 percent of the standard silicon device population.

^{*}The single exception in this model is microwave class devices. Because of their very low power rating, the preferred model is divided into three power categories. With few data available on transient failure of microwave devices (the standard silicon device population contains one microwave device, the lN2lWE), the best that can be done with the present study is to exclude this category.

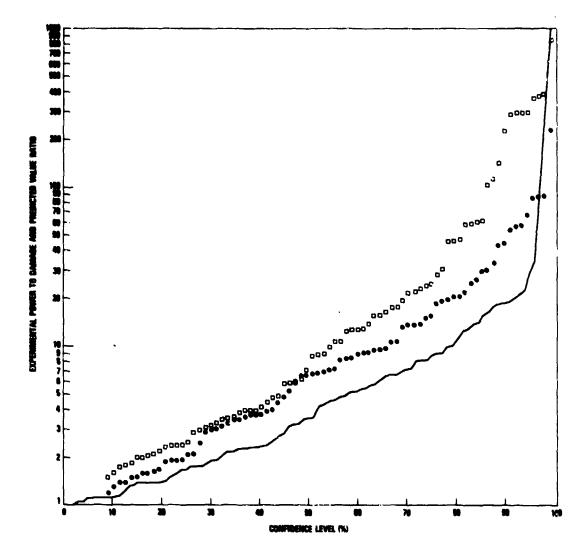


Figure 9. Confidence level for dc power rating model: arithmetic mean used as standard for developing model parameters (solid circles), median values employed (squares), and confidence level for junction capacitance damage model (solid curve).

In the development of this model, the same assumption on the power relation of equation (1) is employed as in the junction capacitance damage model (N = 0.5), despite the results of figure 1. In this way, the comparison between models minimizes this factor as a source of error and allows a better comparison between the basic damage models. The model is developed by averaging the experimental powers to damage at the $10-\mu s$ pulse duration for that segment of population A applicable to this

model as previously defined for the high power class and low power class of devices. The average is defined, as previously, as both the arithmetic mean and median values. The Funsch-Bell relationship of equation (1) is used to calculate the effective damage constant for the high and low power devices:

$$K_{\rm H} = 3.16 \times 10^{-3} P_{\rm H}$$
 (12)

and

$$K_{\rm L} = 3.16 \times 10^{-3} P_{\rm L}$$
 , (13)

where K_H and K_L are the damage constants for the high and low power class of devices and P_H and P_L are the corresponding average experimental power to damage at 10 μs for population A devices. The values for K_H and K_L are given in table 3. Using equations (12) and (13) with the damage constant values of table 3 on population B devices results in the confidence level curves of figure 10 (with the junction capacitance damage model curve included for comparison). There is no appreciable difference in the predictive capability of the junction capacitance damage model and the power class damage model. Included in figure 10 is a fourth curve that represents the scatter in the experimental damage data for all population B devices. This curve is the percentage confidence level that a device selected from among the population B test items has a scatter from the experimentally established damage curves less than or equal to the ordinate value.

TABLE 3. DAMAGE CONSTANTS FOR HIGH AND LOW POWER DEVICES FOR POWER CLASS DAMAGE MODEL

Statistic	Damage constant (W-s1/2)		
	High power	Low power	
Ar + thmedic mean	6.1	0.089	
Median	2.2	0.063	

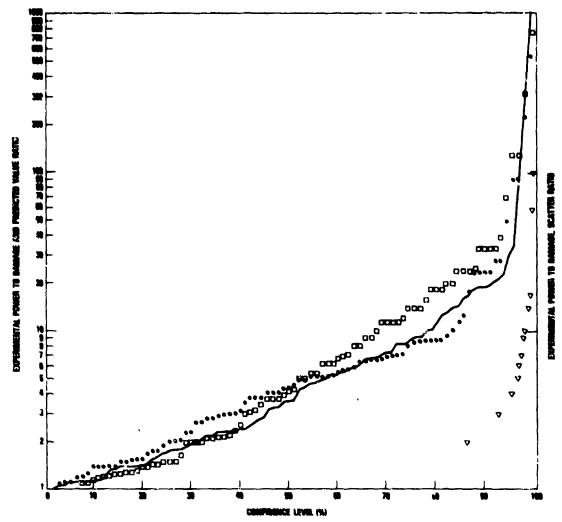


Figure 10. Confidence level for power class damage model: arithmetic mean used as standard for developing model parameters (solid circles), median value employed (squares), confidence level for experimentally established damage curves based on scatter in experimental data (triangles), and junction capacitance damage model confidence level (solid curve).

4. SUMMARY AND FINAL ANALYSIS

Two standards were used to analyze the predictive capability of the junction capacitance damage model. The first was a comparative test based on the development of two alternative, simpler models. Ease of use and general applicability were the criteria for the design of the do power rating and power class models. These criteria resulted in models

applicable to 88 and 90 percent of the devices of the silicon standard population based on manufacturers' published data compared with 16 percent for the junction capacitance damage model. The dc power rating model was based on the assumption that there exists some measure of correlation between transient level to failure and dc power rating. Since certain classes of devices are rated for forward bias and others are rated for reverse bias, no distinction was made between these conditions for model development.

Despite this nonrigorous mixing of power rating standards, the resultant model provided a level of correlation with the experimental damage data only two to four times poorer than the junction capacitance damage model. The power class model was based on the assumption that all devices (excluding microwave diodes) could be equated to either a high power device with a damage constant of 6.1 W-s^{1/2} (arithmetic mean) or a low power device with a damage constant of 0.089 W-s^{1/2} (arithmetic mean). To establish the applicable class for transistors, the manufacturers' catalogings of devices as high or low power were used. Since the dividing line between high and low powers is a rating of 1 W (with some exceptions), the 1-W power rating was used to divide diodes into the applicable classes. The resultant model displayed a level of correlation with the experimental damage data comparable to the level of the junction capacitance damage model. These results do not bode well for the ostensibly more sophisticated junction capacitance damage model.

A second standard to test the predictive capability of the junction capacitance damage model is based on the uncertainty in the failure level of devices resulting from their spread about an experimentally established damage curve. This uncertainty compels the user to place error bars upon the experimental damage data. Also, this uncertainty gives an absolute standard for comparing the junction capacitance damage model. It is standard procedure to define a device failure curve and to bound the lower limit on this curve with a second curve. This lower limit insures a certain measure of confidence that the subject device does not have an actual failure level below the value used. To achieve this same measure of confidence by using predicted failure based on the junction capacitance damage model requires a spread in the low bound approximately one order of magnitude larger than that required of an experimentally determined failure relationship.

In the development of the dc power rating and power class models, some concern must be given to the possibility that the population selected and the standards used produced a fortuitous correlation with the capacitance model. Although the size of the population and the standards used would seem to minimize this possibility, it is a worthwhile exercise to redefine the population and the standards to observe the resultant variation in model predictions. An exhaustive

compendium of such results is given in the appendix. A rigorous comparison among the many predictions is difficult because of the varying standards. Nevertheless, the trend indicates a variation in model predictions, particularly for the power class model, that requires no qualification of the results given in the body of this report.

APPENDIX A. -- DAMAGE MODELING COMPUTER CODE

Contained within this appendix is a code used to generate many of the data presented in the body of the report and a statistical study of the direct current power rating and power class models based on varying population standards. Included with the code is a single printout of resultant code data. The printout covers only those data for which the arithmetic mean was used for all modeling, and the extrapolated values for experimental power to damage were incorporated into the data base.

Although not indicated in the main body of the report, a study of the performance of the junction capacitance damage model for germanium devices is included. The germanium device model was taken from documentation receiving limited distribution based on a very limited germanium device population. Predictably, the results indicate a much poorer performance of the junction capacitance damage model for the germanium than for the silicon devices.

The nature of the populations and the results for the alternative tests of the proposed models are discernible from the information included in the data output. The quantity of the printed data is indicative of the mass of the data that must be handled in a study of this nature.

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```
6 CONTINUE
CALL SUBJECT. 33. C(2.31, C(3.31, Mal. 13, 31, VAL. 12, 3), VAL. (3.31)
C VAL. (1.31) - (2.31) - (2.31, C(3.31, Mal. 13), VAL. (2.31), VAL. (3.31)
CD 26 M-13.3
CD 27 M-69.61
IF (A. (M. M.) - (1.61) - (1.61) - (1.61)
IF (A. (M.) - (1.61) - (1.61) - (1.61)
IF (A. (M.) - (1.61) - (1.61) - (1.61)
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CALL SUBSCELL-23,21,6(2,2),6(3,2),841(1,2),841(2,2),841(3,2))

CAL(1,2)-(2,2)-(3,2) ARE CONSTANTS FOR ALL SILICON DEVICES
CALL SUBATKA.B.M.C.IM.27,KC.PREDCT 3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         SUBBITA BONG (M.3), KC. PREDCT !
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     A (M.) MI) - 4 (M. M.) / 4C (M.) 31 - A (M. 4.) 1
CD#1 1MUE
CORT SRUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              DD 5 4-1-66
If (A(M.61-60.0.) CD TD 5
IF (A(M.M.60.0.) CD TD 5
IF (A(M.M.60.0.) CD TD 5
IF (A(M.M.61-60.0.) CD TD 5
IN-21-APT AMM/A (M.61-60.0.)
CM, 21-6PT CDM TMUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            DG 24 M-1,3
DG 25 M-1,46
If 66 66,61,60,1 GG 7G 25
If 66 10,61,60,0,1 GG 7G 25
MM-4,0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          16 (54TCH-EQ.O.) 60 10 312
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   91*1.+97
CONTINUE
C(M, 3) *C(M, 3)/97
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  332
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34
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16 STOTCH-EG-0.1 GG TG 313

17 STOTCH-EG-0.1 GG TG 313

18 STOTCH-EG-0.1 GG TG 313

18 STOTCH-EG-0.1 GG TG 314

19 STOTCH-EG-0.1 GG TG 314

10 STOTCH-EG-0.1 GG TG 314

10 STOTCH-EG-0.1 GG TG 314

10
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36

```
CALL SUB(C(1, 4), C(2,4), C(3,6), VAL(1,4), VAL(2,6), VAL(3,6)]

VAL(1,6)-(2,6)-(3,6) ARE CONSTANTS FOR GF DEVICES MITHOUT CAP. MOSEL DATA
DO 35 M=6,9]

IF (A(M,N)-EQ-0.) GO TO 35
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       SUBA EKA .E .M.C (M.7) .KC . SHTCH)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    [ H, MN] "A (M, M) / (C (M, 6) "A (K, 4)]
                                                                                                                                                                                                                                                                                                                                                                                           C(W, 6) D(KK)

60 70 12

D0 13 K=69.91

17(A(W, 6) .EQ.0.) G0 T0 13

17(A(W, 6) .EQ.0.) G0 T0 13

17(A(W, 6) .MC 0.) G0 T0 13

17(A(W, 6) .MC 0.) G0 T0 13

A(W, 6) .MC 0.) A(W, 6) .MC 0.0

PT = 1.00T
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           GD 10 14

DD 15 N-1,31

IFA(N,6) -EO.,1 GD 10 15

A(N,N) -EO.0.1 GD 10 15

A(N,N) -AFS(A(N,N))

C(K,7) -A(N,N)/A(N,6) -C(N,7)

PT: 2.97

CONTINUE
                                                                                                                                                                     BG-0.

D(RK):0.

D(324 N=69.91

IF(A(N=6):E0.0.) (O TO 324

IF(A(N=0):E0.0.) 60 TO 324

IF(A(N=9):ME.0.) 60 TO 324

IF(D(N):LE.BG) 60 TO 324

IF(D(N):LE.BG) 60 TO 324
MM-1+MM
IF PREDCT.ME.O.P CD TO 6.2
JF (BRIM.M).LT.0.) B(M.M)=0.
CONTINUE
CONTINUE
CONTINUE
MMB-MM/2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                DO 14 H=1,3
1F(SWTCH.EQ.O.) CO TO 325
KA=31
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       14.62-C(M.63/PT
                                                                                                                                      KK-92
DO 323 K=1,NNN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   328
                                                                                                                                                                                                                                                                                                                                                                       324
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37

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CONTINUE

CALL SUB(C(1,7),C(2,7),C(3,7),VAL(1,7),VAL(2,7),VAL(3,7))

CALL SUB(C(1,7),C(2,7),C(3,7),VAL(1,7),VAL(2,7),VAL(3,7))

CLI,T,T,T,C(2,7),C(2,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,7),C(3,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CALL SUBATRA BONGCIMISTORC, SHICH)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   SUBA (KA .8 .N.C (M.9) . NC . SHTCH)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DO 40 K=76.91

|FF4KK,K1.EG.0.1 GO 70 40

|FF4KK,S1.20.1 GO 70 40

|KERKY.27

|KERKY.K1.4KK,K1/4C(K.8)+AkK.61

|CDNTRUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 00 19 A=32.68

IF (A(N+6)-E0.0-) ED TU 19

IF IA(N+N)-E0.0-) GD TO 19

A(N+N)-APSIA(N+N)

C(M+9!=A(N+N)/A(N+6)+C(N+9)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                IF(A(N.6).FO.0.1 GO TO 16

IF(A(N.N).EQ.O.) GO TO 16

A(N.N).ABS(A(N.N))

C(N.8).A(N.N)/A(N.6)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             0 10 M=1,3
FISHTCH-EQ.O.F CO TO 327
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CONTINUE
DO 17 M=1,3
IF(SWICH-EQ.O.) GO TO 326
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       14.91-CIR.93/PT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           14,80 H 3 D = (8.8)/PT
T4/17, 413=15, 412
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          S C VALE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            327
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#11H 1 USEC #11H D-1 U
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     ,11H 0.1 USEC ,11H 10 US 10 USEC ,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             IEC ,11H 0.1 USEC ,11H 10 USEC ,11H 1
IH 10 USEC ,11H I USEC ,11H 0.1 USEC
1 USEC //!
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    MRITE(6,210)DEVICE(MA),DEVICE(MB),DEVICE(MC),DEVICE(MD),
E(MIM,M),M=7,16)
FORMATIEM,444,10F11,5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   MAITE & 210) DEVICE HAD DEVICE HA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               KD-4.4N-13-4
Writtl.21010Evice(Kaj.Device (Kaj.Device (Kaj.Device (Kc).Device (Kd).
[18/N.J.N.27.36]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ##1FE46,291)
FORMAT(2216,114 0.1 USEC ,114 10 USEC CSEC ,114 10 USEC ,114 1 USEC ,114 0.1 USEC //)
                                                                                                             IF(A(M,4),E0.2.) &D TD 512
IF(A(M,H),E0.0.) &D TO 512
A(M,MH)=A(M,H)/(A(M,4)°(S)
A48,MH)=A48,H)/6A48,5)+C5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   MRITE(6,214)
MRITE(6,254)
FORMAT(22x,119
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WRITE(6,888)
FORMATIZX;104HN VALUE FOR RELAFIONSHIP: K=PoTood-N) DERIVED FROM
Experimental Damage Data for time intervals indicated//)
Write(6,830)
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britel6.251)Device(KA),Device (KB),Device (KC),Device(KD),
& (SLOPE(N,M),R=1,3)
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[6,1121][C[M,3],M=1,3]
[6,1121][C[M,5],M=1,3]
[6,1121][C[M,6],M=1,3]
[6,1121][C[M,6],M=1,3]
[6,1121][C[M,6],M=1,3]
[6,1121][C[M,6],M=1,3]
[6,1121][C[M,6],M=1,3]
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AC-4-0[N-1]+3

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MRITEGE-5-5-02-10EVICE-[KA], DEVICE-[KB], DEVICE-(KC], DEVICE-(KD],

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DO 401 N=NC,ND
IF (PWR(N)-1.) 401,402,403
DD=1.+DD
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IKK-21361,362,363
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TO 360
381 NZ=1,91
R(NZ)=PWBA(NZ)
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413 R=37,45
N=M1=0-
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375 CONTINUE
C FOR PURB: SAME AS PURA EXCEPT LIMITED TO DEVICES MITHOUT CAPACITANCE DANAGE
C MIDEL DATA
MRITECO-214!
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350 FORMATGZX-125HD= EXPERIMENTAL POWER TO DAMAGE/KA+T++4), WHERE K
                                                                  SUBSTADD ACC OU MC OND PUR PHAL PERHI
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|F(KL-EQ-1) GO TO 450
|F(PWR(K)-ME-L-) GO TO 344
|MR-MN|=PWR(K)
                                                                           60 10 408
D0 340 N=NC,ND
IF(PWN(N)-1.340,341,342
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DG 461 N=MC.ND
PAR(N)=PARB(N)
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XP=100,+2,512++(H-1)
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FORMATIZATIZSHP. EXPERIMENTAL PONER TO DANAGE/KAPIP-53. WHERE R
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Edevices)
LA DAPAGE CONSTANT BASED ON HIGH POWER OR LCW POWER RATING FOR ALL
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CCAPACITANCE DAMAGE MODEL DATA)
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     MEITERG.3528
FORMATIZX,43MQ=SAME AS D EXCEPT FOR SILICON DEVICES ONLY)
MRITERG.3539
FORMATIZX,43HR=SAME AS P EXCEPT FOR SILICON DEVICES GMLY)
MRITERG.3541
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KA = 4 = (R = 1 ) + 1

KB = 4 = (R = 1 ) + 2

KC = 4 = (R = 1 ) + 2

KD = 4 = 4 KB + 1 + 3

KD = 4 + 4 KB + 1 + 3

KD = 4 + 4 KB + 1 + 4 KB + 4 KB
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ta-3591 dev i ce i kal "Devi ce (KB) "Devi ce (KC) "Devi ce (KD) "
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DO 371 N=1,91
KA=40(M=1)+1
KB=4-(N=1)+2
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MAITEIO-2001
FORMAIESX,59HQUANTITIES A THACUGH JAND L THADUGH Z DROERED BY MAG
EMITUDE////)
FORMATICEX, 82 HZ = SANE AS T EXCEPT MUCC. LIMITED TO DEVICES WITHOUT CCAPACIDANAGE MODEL DATA//)
MRITE16,306)
FORMATICEX, 11H U , 11H
                                                                                                                                                                                                                                                                                                                                                                                                                                        LIIM W .11M W .11M W .11M W .//!

MRITE(6.357)

DG 349 M 1.91

KR + 4 + 6 M - 1 + 1 + 2

KR + 4 + 6 M - 1 + 3

KR + 4 + 6 M - 1 + 3

KR + 4 + 6 M - 1 + 3

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KR + 4 + 6 M - 1 + 3

KR + 4 + 6 M - 1 + 3

KR + 4 + 6 M - 1 + 3

KR + 7 M - 1 + 3

KR 
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KD-4-0(h-1) +4
ARITE (h-359) DEVICE (KA) , DEVICE (KB) , DEVICE (KC) , DEVICE (KD) ,
G (ARI, M) , M = 73,81)
COMTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           NAAZ-NAA
CONTINUE
CONTINUE
IF 686.E0.0.1 GO TO 299
AIRZ:NAAZ?-0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                DD 394 N=1,91
DD 394 N=1,91
A(N,F)=ABS(A(N,H))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              MRITE(6,214)
WRITE(6,391)
FORMAT(22X,11H
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      V(N,N)=A(N,N)
CONTINUE
DO 299 N+1,25
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     26
45
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                                                    38.7
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NATTEE 6.305) (SCN.M).M-1,KK)
FORMATCAY.10F13.5)
IF (KANC.NE.1) 60 TC 327
MRITEE 6.726)
FORMATCAY.57MPARANETERS IMMEDIATELY ABOVE WS PER CENT CONFIDENCE L
MRITE FG. 4121
FORMATESX, 36HSILICCH DEVICES UNLT FOR L. M. AND N///)
IF GGABC.NE.11 GO TC 424
MRITE FG. 4251
MRITE FG. 4251
FORMATESX, 106HFUR VALUES OF A THROUGH J AND L THROUGH Z LESS THAN EL, WALUE TABULATED IS INVERSE OF THE VALUE LESS THAN 1///)
CONTINUE
DO 304 M.=1.25
DO 484 K.=1.273
IF ESK.#H1.EQ.().1 GO TO 485
KK.=1.45K.#H1.EQ.().1 GO TO 485
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           ##ITE(6,731)(CMT(LM),LØ=1,kZ)
FORMAT(2X,F9.2,F5.1,4X,F9.2,F5.1,4A,F9.2,F5.1)
L4X,F9.2,F5.1,4X,F9.2,F5.1,4X,F4.2,F5.1,4X,F9.2,F5.1)
(ONTHUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       RABC = 1 + KABC

IF (KABC = KE = 1) GO TO 422

DO 423 M = 7 + 81

DO 421 M = 1 + 92

IF (V (M + N) - 6E - 1) GL TO 4 E2

IF (V (M + N) - 6E - 0 - 1) GO TO 4 B2

A M + N + 1 - V (M + N)

GO TO 421
                                                                                                                                                                                                                                                                                                                                                            PERCATIKL)=( (AK-AL) *100.1/AK
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CAT (KZ) =PERCAT (KT)
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          00 480 N=1,255
00 481 N=1,273
5(N,M)=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             WRITELS,3061
FORMATIZX////
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                            KZ=1 0KZ
CNT (KZ)=5 (KT pP)
KZ=1 0KZ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                A(N, M) = V(N, M)
CONTINUE
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                           00 730 KR=1,KK
KT=1+KT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             - C-
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  121
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421
420
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          774
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                                                                                                                                                                                                ;;
                                                                                                                                                                                                                                          3.15
                                                                                                                                                                                                                                                                                                                                                                                    729
                                                                                                                                                                                                                                                                                            726
                                                                                                       45
                                                                            425
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50

RATIO OF EXPERIMENTAL PLUER TE DAMAGE TO DE POWER MODEL PREDICTED VALUE FOR FOLLOWING MODEL DATA BASES

A..ALL DEVICES

B..ALL SILICON DEVICES

C..ALL GERMANIUM DEVICES

C..ALL GERMANIUM DEVICES

E..ALL SILICON DEVICES MITHOUT CAPACITANCE MODEL DATA

E..ALL SILICON DEVICES MITHOUT CAPACITANCE MODEL DATA

F..ALL SILICON DEVICES MITHOUT CAPACITANCE MODEL DATA

G..ALL SILICON DEVICES MITHOUT CAPACITANCE MODEL DATA

M..ALL SILICON DEVICES MITHOUT CAPACITANCE MODEL

I..ALL SILICON DEVICES MITHOUT CAPACITANCE

J..ALL SILICON DEVICES MOT INCLUDED MITHIN 145 REPORT

J..ALL SILICON DEVICES INCLUDED MITHIN 145 REPORT

FOR ALL CASES WHERE DATA BASE PERMITS. RATIOS ARE DHLY FOR THE REMAINING SILICON OR GE DEVICES NOT INCLUDED IN DATA RASE

A 0.0 ENTRY INDICATES NO DATA OR NC CALCULATION

FOR ITEM K. -1 INDICATES NO CALCULATION

REGATIVE SIGN INDICATES ESTINATED VALUES FOR POWER TO DANAGE JUNCTION REVERSE BIAS CONDITIONS ONLY

ARTIHMETIC HEAN JSED FOR ALL MODEL DATA BASES

ALL PREDICTED VALUES FUR EXP. PUWER TO DAMAGE INCLUDED IN DATA BASE CALCULATIONS

	EXO. BOMED	64m2 - 674		DAM CONST.	DAM COMST		PONE CLASS
	TO DANAGE	TO DANAGE AT 1US	TO DAMAGE AT 0 -BUS	52	. 5 5	-	K164-2
SALICON DESIGNS	(NATTS)	(WATTS)	(MATTS)	(N.SEC5)	(N. SEC 5)	(NATTS)	E X CL UD ED +0
284 C-	20.000	\$2.000	140.000	3.2300	0.8 470	0.4000	-1
2N32BA(t-8)	.01.0	16.000	30 .000	0.0	0.3300	0.4000	7.
24335 (C-F)	20.000	000-00	300 000	0.3050	000000000000000000000000000000000000000	0-1800	
2H3365JAN1C-0)	30.000	70.000	160.000	0.4500	20.0	0.1500	
P	75.300	112,000	625.000	0.0	0	0.1500	:_:
2N24841(-D)	42.000	946 - 300	20 -000	0.0	ر•(0.3600	-:
242484(F-B)	15.000	000 . 84	160.000	ع د د	0	0.3600	۵.
2437445 AB		000.27	113,000	200			• ~
	000.04	000-47	000-041	90.0			•
24933 (E-B)	16.000	000.09	230 000	0.0	0.010	00000	
2N2481(C-E)	10,000	10.000	10.000	9.2530	4.3930	0.3400	-
242401(E-0)	16.000	30.000	53.000	0.0	0.1240	0.36.0	
2N2 90 7A (C - D)	20.000	23.000	135.000	.	0°0	0004-0	
242967A (E-B)	53.000	16.000	110 .000	0.0	0.0	0.4000	∴ .
2N222A(C-6)	32.000	35.000	220.000	٠ • •	50	9000	•
787787	200-001	000-002	000-0046) ·	20.00		
F 5911 -3465	00-00	, ,	4100-000	0-0	27.7000	q	
14816	9	2700.000	00	0.0	1.9300	0.0	~
112146	1.100	2.000	3.400	0.0	0.0	0.0	•
18914A	15.000	90.000	420.000	0.233	0.4230	0.0680	
A 2 C M 1	000" £ 3	340-000	2300 0002	0.0	0.5360	0005-0	.
PC115	510.000	1350.000	3300.000		0.0	9.0	.
14302 00 13 00 N	000.0001	966-61166-	000 0000 1-	3 6	24.5000	0000	•,
123005A	-26244.594	000-0006	262446 .000	0.0	0000	10.000	; ;
143016	13000.000	41079.996	-130000.030		23.1930	•	7.
196141	300.300	-25279.996	- 80000 - 000	0	16.1000	3.0000	~
1002	900.074	-2117-200	00.0 € 00L 9 -	ر. • -	17.7036	0056-0	7:
2N2057(C-B)	12.400	16.000	120.000	0 0	0.0	0.2000	•
2N2057(F-B)	0.040	009.2	06.2.8	e e	0.0		
19-112/12/13 24224/4/19	090 000	1000-000	1900-000	2		0000-11	; ~
28.22.24E-27	100.000	7 100-000		0	0.0	75.0000	. ~
	1300.000	3800.000	13000,000	0.0	0.0	75.0000	~
2N3584(C-B)	120.000	370.000	1200.000	0.0	0.0	2005	
78356466-6	۰ د	2150-000	88	ت - د	÷ 6	٠	∴ .
10-11-60747	2000	200	0000	2 0) C	0046	•
245824(C-8)	4 4	17.000	47.000	0 0		• •	: .:
2N5629(F-6)	4.300	10.000	22 -0170	} ?•	<u>.</u>	0.02.0	::
2N30135JAN(C-0!	4	21.000	100 • 000	0°0	0.0	0.3400	
2N3013xJAN (E-B1	20.000	31.500	52.000	0.0	0.0	0-3400	
CA3016(C-0)	009.5	20.000	000	9500*0	٥•٥	ů,	<u>.</u> .
(A3016(E-B)	90.4	10.00	ე(: 0° 22 : 25	1 0.7. 0	- ·	000E* 0	. ;
SHB52-6517-6-81	26.000	202-001	320,000	0 3	0 7	0 7	• 6
2414138446 [C-6]	000-0071	2100-000	3200-000	0.3016	08480	0000	
2416132AN(F-81	160.000	. ~	750.000	-	0.1030	0000	: -:
2414858JANIC-BI	100.000	1100,000	1 700 -000	0.0	0.0	1.7000	?
2N14B58JAN(E-B)	3100.000	-30000-600	000-000162-	0.0	ر • ع	1.7050	2.

18-31817636	020-01	27.0010	74 - 41:30		•	1.3900	2.
283439(6-8)	160.000	620.000	2200-000	0.0	0.0	1 .0000	7.
2N706 SJAMIC -9 3	2.800	17,000	93.000	0.0243	0.0	0.3000	-
247065JAN(F-B)	9.00	16.000	000-05	3.0	0.0	0.3000	1.
18-69-6735	750.000	7500°000	75.JOG . DOL	0.0	0.4	7.0	÷
1N2500	17000-000	-53719.996	-170000.000	0.0	0.0	13.0000	7.
IN751 ASJAN	240.000	2500.000	25500,000	0.0	3.33.10	0.4000	:
10485B: JAN	100,000	435.000	2000-000	ن • 0	0.6110	0.2500	-
1M2991813AM	100000	-31599.996	-100000-000	ે •	28.00.13	10.0000	2.
1 M 3 0 2 5 B 5 JA M	1400,000	-14000-000	-140000.000	0.0	7.4600	1.0000	2.
MD1054	25.000	33.500	000-44	0.0	0.0	0.0	•
18746AS JAN	2600,000	-20000,000	-153800.000	0.0	3.4400	0.4000	-
18645 5.JAN	, O. • O. •	580.010	1625.030	0.00	3.6 300	0.4000	1.
INI 20 2RAS JAN	100.000	1000,000	9000.000	0.0	0.0	12.0000	7.
INI TOTALAN	600.000	2000-000	5700.000	٠ <u>٠</u> ٥	0.0	7.3000	?
SECULOR DEVICES			•				
244C4A1C-83	120.00	160.000	230 - 000	0.0920	6. 61. • I	0.1500	-
2M404A(E-B)	104.000	140.000	175.000	9	0.6490	0.1500	:
2M297A(C-B)	2000.000	22 10,000	2700-000	0.0	55.60JD	35.0000	2.
2H297A(E-B)	1400-000	2100.000	3300.000	0.0	39.5000	35.0000	2.
24526 (C-B)	130.00	225.000	425.000	3 9 9 1 5	2.39:	0.2250	-
2N526(E-B)	160.000	290.000	200-000	0.0	1.9200	0.2250	-
1M270	19.00	20.000	23.000	(*0	1.3600	00000	-
2N396A1C-01	115.000	170.000	230.000	0.0870	0.0	0.2000	-:
2N396A(E-#)	13 / 100	0€0°€1.2	350.035	ت. د.	•	0.06.0	
2M4.28 M1.JAN (L-B)	170-000	260.000	420.000	0.0670	0.0	0.1500	-
20428MEJAN (E-B)	220.00.	200,000	335.000	0.0	ა • ი	0.1500	-:
	300.000	1100.000	3400.000	0.0139	0.0	0.0350	-:
2K393 1JAN(E-B)	33.100	160-03.	7-19 - 000		5.05	0.0380	-:
2N501 A: JAN(C-8)	3.000	17.000	000.48	0.0113	0.0	0.0600	-
2N501A1JAN(E-B)	, 0 6- 7	18.000	79.000	(°, n	G*0	00 90 °C	:
2N7CS EJANEC -B)	7.800	15.000	30 -000	6.0363	0.0	0.1500	:
	3.665	6.69.0	12.000	ن. دو	~ .	0.1500	-
2 M466 M2 JAN (C-B)	470.00C	000-000	1400,000	0.5690	0.0	0.1500	-
	0.00	290-000	930.000	ا: م	ĵ. ° 0	0.1500	1:
2N1042RAJAN (C-8)	200.000	1500.000	4000.000	0.0	0.0	20.000	3.
2M1C42RAJAN (E-B)	361-160	17.0.000	75v0.v	2) • t	20.0000	7.
18277:JAN	14.000	18.000	23.000	0.0	0.0459	0.0800	-
MS1.40	004.0	0.440	0°5°0	Ú.,	0.0072	000000	•

RATIO OF EXPERIMENTAL PUWER TO DAMAGE TO DEVICE OF POWER RATING

35%	75.0	2,000.5	1000	1066.7	4166.7	136.9	4.444
130.0	0.04	533.3	293.3	4.66.7	746.7	127.8	133.3
20.0	\$2.5	133.3	133.3	20C •)	4.66.7	116.7	41.7
2N328A1 (-8)	2N320A(1-3)	2N335 (C-B)	2N335(E-B)	2N336 EJAN(C-B)	2N334 EJAN(E-61	2N2484[C-B]	242484(1-4)
	50.1 130.0	50.) 130.0 22.5 40.0	50.1 130.0 22.5 40.0 133.3 533.3	50.) 130.0 22.5 60.0 133.4 533.3 133.3 293.3	50.) 130.0 22.5 40.0 133.3 5 533.3 133.3 2 93.3	50) 130.0 22.5 40.0 133.3 133.3 293.3 20() 466.7	2N320A(C-B) 50.1 130.0 357.0 2N320A(C-B) 22.5 40.0 75.0 2N335(C-B) 133.3 593.3 200.0 2N335(C-B) 133.3 20C.) 406.7 1066.7 2N33512AN(C-B) 20C.) 406.7 1066.7 2N3454(C-B) 116.7 127.8 138.9

230.0	.0 1189	• •	3	.72	171					000	.2	0	0	0	.5 6176.	575	. 000071- 0	70001- 0	-26244	-130	6.7 -2666	1.52	0.0	3.63	1401 411	7-0	173.	-085 0-8	. CD()* n.	.9 672	235	110.	.3 277.	.5 144.	. 613.	.0	0.0	•	5.0 937	1.1	7.0 78.	0.0 2200.	6.7 310.	100	2.3 -13076	0.0 63750.	.0003 0.0	0.0 -10000.	0.0 -140000.	0.0	0.00 -384500		
41 0 0	20.0	57 0.	.3 20	7.1			2.0	61 .	0.0	17 (100)	2.4	÷.	ę	0.0	.6 117	07.5 85	0.0	316C 0.000	383.8 138 626.5 -830	217	2666.7 -842	705.3 -222	2.0	7-5	. a		2.0	14	9.0	6.0	n	200		5.6		7	9	1750.0 262	0.00	9.11	0.0	•			7	0.00	7 0°C	-316-	400 °0 -140	0.0		0.00	
N37361(-B)	-	N930 (C-8)	3)(1 87		31100		NZ9)7A(E-B)	N222241-81	M2222A(E-B)	24384	5911-3465	Ma16	N2 14E	-	š	15	9 •	7 7 9 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9	_	2001		1857(E	9	4908JAN(C	3	31465	15841E	31469	1)561	12966	10131JANIC	10138	31010	197691	, z	161 3EJANIC	61 32 JANGE	- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4875JAN	14396	AL 1 407	A SJANIE -B	70.00	75141JA	151	131164	102581JA	131054	18746.88 JAN	545 EJAN	

	0 10 USEC	0.000000000000000000000000000000000000
	C USEC	
	C 3 USEC	
	C 10 USEC	
	B 0.1 USEC	0.01148 0.09390 0.09330 0.09330 0.09330 0.01220 0.01220 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139 0.0139
	B 1 USEC	0.03411 0.013994 0.13994 0.12245 0.13298 0.03498 0.03498 0.03498 0.03498 0.046412 0.04681 0.04681 0.04681 0.04681 0.04681 0.04681 0.04681 0.0528 0.05
	B 10 USEC	0.05073 0.13529 0.13529 0.20293 0.4228 0.08929 0.65411 0.08929 0.65411 0.08929 0.05073
1533.3 1166.7 77.1 1166.7 1188.9 2222.2 2222.2 2223.2 287.5 1150.0 1150.0 2000.0 2000.0 2000.0 2	A 0.1 USEC	0.02147 0.00460 0.12269 0.06543 0.06543 0.02226 0.01231 0.01231 0.00170 0.0017
10.00 10.00	A 1 USEC	0.03766 0.1559 0.156497 0.13518 0.03862 0.03862 0.03862 0.05793 0.05793 0.05444 0.05793 0.05444 0.05793 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.054444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.05444 0.054444 0.05
693.3 693.3 57.1 711.1 237.5 711.1 711.1 711.1 711.1 711.1 85.0 80.0 94.0 96.0 96.0 96.0 96.0 96.0 96.0 96.0 96	A 10 USEC	0.04975 0.13266 0.13266 0.13266 0.132663 0.13663 0.06755 0.076766 0.079766
2N444A(C-B) 2N597A(C-B) 2N597A(C-B) 2N596(C-B) 2N526(C-B) 2N526(C-B) 2N526(C-B) 2N526(C-B) 2N536A(C-B) 2N596A(C-B) 2N596A(C-B) 2N5981AN(C-B) 2N5981AN(C-B) 2N5081AN(C-B)		2N328Aff-8) 2N328Aff-8) 2N328Aff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N335ff-8) 2N235ff-8) 2N235ff-8) 2N235ff-8) 2N23736ff-8) 2N2464ff-8) 2N2524ff-8) 2N2524ff-8) 2N2525ff-8) 2N3525ff-8)

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4 4 6 6 6 6	01110	2 40420	•	2.66291	2.17778	.31	0.0	0.0		7.69997
44.00	12 934.24	11 80080	. 5	13,19046	10.77870	4	0.	0.0		30141.00
120100	2 6531	20074		2.70573	~	E	0.0	0.0		1.82340
1 + 1 + 1	07 FOR 0	4466	74757	0.71560	0.58476		0.0	0.0		2.06919
	2101.0	0.04000	0.000	0.420	000000	3	0.0	0.0		0.0
12857(C-8)	69190°0	1620-0	100000	40000	17500	5	0.0	0.0		0.0
	0 -00418	77500-0	767000	0.00428	10000	0.00817	, c	0.0		0.0
	7764(*1	0.01.003	1001010	0.000	0.010.0	ě	0.0	0.0		0.0
M3375(F-B)	0.0000	46410-0	66.000.0	7.4500	0.00805	0.00466	0.0	0-0		0.0
	0.000	84410-0	0.01063	0.01759	0.01329	0.00866	0.0	0.0		0
	0.04776	0.04287	0.02945	0.04870	0.03683	0.02398	0.0	0		9.0
N3584(F-8)	0.19501	0.24912	0.24538	0.19887	0.22565	0.19979	0,0	0.0		
	0.03869	0. 14023	0.32897	0.03946	0.03644	C-02359	و د د	9		2 6
42894(E-B)	0.03316	0.01529	0.00511	0.03302	0.01385	0.00416	0 0	2 0		200
N5829(C-B)	0.02985	0.02462	0.01442	0.03044	0.02230	3 6	2 0	•		0.0
N5829(F-B)	0.02139	0.01448	0.00675	0.02181	0.01312	V-C00.0	9 6			0
	ं ा 188	Ś	0.01704	0.01212	16610-0	2 6	2 0			0.0
N30131JAN (E-B)	0.05527	0.02535	99800	0.05637	770	2 2 2	200			0.05672
A3018(C-B)	0.01924	0.01931	001300	1962	0.00875	0.00366	000	0	0.0	0.03912
A3018(E-6)	0.01327	9600.			=	0	0.0	0.0	0.0	o. 0
MB 526517(C-B)	ې ت د	- C			0	0.0	0.0	o - 0	0.0	0.0
MB 32 03 1 7 1 E - B 7	1.74115	0.76039	0.24538	1.77564	0.68876	0.19979	0.0	0	0.0	5.13437
M 1 G 1 J 2 J 3 R 1 C - G 1	0.108.00	231	0.05751	0.20293	0.11151	0.04683	0.0	0.0	0.0	6.58679
2101747747 21487748	9960-5	0.18744	0.06134	0.4178	0.16978	0.04995	Ç.	0	0.0	2
MICHSTANIE-B)	1.01431	8	10.46465	1.85024	4.63029	8.52059	0.0	0.0	.	9
K3439(C-B)	\$660C* C	0.30782		0.01015	0.00708	0.00390	٥ رو ر	0 0	200	•
N3439(E-B)	0.17909	36	0.13496	0.18264	0.16268	0.10989	0,0	9 0		AF7 50.0
N706 : JANIC - B)	0.60929	\$.) •01902	0.00947	19910	0.01348	2 0	9 6		0-0
N706 : JAN(E-B)	0.02255	0173	0.01022	0°50°0	0.01574	0.00832	200	•		2 0
R-69-6735	င္	٠ •	ر. د	2	٦,	0.0	2 0	9 0	2 0	0
N2580	1.30108	1.19702	0.80220	1.32685	1.08425	0.65317	200	0.0	90	1.76635
N751A:JAN	J.59697	8194	1.016.6	V 800 4 0	6 4	0.1995		0	0.0	1.17357
N4858:JAN	0.39798	5040	9,065.0	0.40360	•	0.400 A	200	0	0.0	2.93392
N299 IB: JAN	96464	9 135	-01044 	4 205	•	6.99276	0	0.0	0.0	4.10749
N30258:JAN	1-39292) () ()			,	0.0	0.0	0.0	0.0	0.0
01054		34.84.96	23.58696	6.59523	916	19.20512	0.0	0.0	0.0	19.070.61
N/40AZJAN R44E + 44E	1 26268	0.42003	0.24921	. ~	9.38046	0.20292	0.0	0.0	0.0	3.66741
N12028451AN	0.00829	0.02414	0.04601	00	187	0.03746	0.0	0.0	- c	
M173145.14R	0.19899	0.14484	7.08742	202	130	0.07118	0.0	2.0	0.0	21746
N404A (C-B)	0.19595	0.30899	0 -09406	0.0		0.0	0.1010	#01ZF-0	0-17679	2.03419
N404 A1 E-B)		0.27036	0.17157	5 0		200	0.05411	0.02499	0.01169	0.16765
N297A (C-B)	0.0000	0.01621	0.000 c			0.0	0.03788	0.02385	0.01429	0.11736
14297A(1-D)	0 57656	0.28967	0.11587	0		0.0	0.54713	0.39754	0.28623	1.69516
1872011-01 1852615-81	1.70751	0.37336	0.13632	0.0		0.0	0.47339	0.51236	0.33674	2.01635
M 2 70	0.23630	0.07242	0.01764	0.0		0.0	0.52490	0.09938	100000	ì
N3964(C-B)		0.24622	0.47055	0.0		0	0.54450	0.33/91	96519	
N396A(E-B)	0.64671	0-29692	0.10735	0.0		9 0	12670.1	0.68906	0.42430	3.32512
18-3 INVE 3H 825N	1.1276	0.50210	0.17176) (1.38846	0.74207	0.33843	
SN428M: JAN (E-B)	1.45925	2.24672	0.13100			0	8.11673	12.49399	14.72055	25.14792
243932JAHI (- B)	8-36-6 6-5-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-	1 22622	1,27689	0		0.0	0.89264	1.01731	3.03070	0
243435JAN(R-6)	F0956-0	77670	18743			0.0	0.04735	0.11264	0.21720	0.14670
CHOOLATION (- D)		0.08690	380	0.0		0.0	0.07733	0.11926	0.19952	٥,
NAC SEJAN(C-R)	517	10-2897	. 1122	0.0		0.0	926900	0.03975	16060-0	0-15/50
NA 105 8 2 AN (E - R)	0.02388	0.01275	0.00491	0.0		0 0	0.02273	0.01/49	1.41433	
MAGENE JANCC B)		5446	.5725	0.0	0 0	0 0	2.76733	2.09369	0.93952	ì
PN466M:JAN1E-B)	4.24509	S.	36.)	· ·		•	1 1 2			1

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ZNIC4ZRAJANIC -BI ZNIC4ZRAJANIE -BI	0-01791	0.02462	0.02300	000	0	20	0.01705	0.03379	0.05683	0
1N2775JAN #51040	0.00663	0.06518	0.00051	3 0	0 0 0	00	0.00631	0.00292	0.00126	0.01956
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	c	¢	•	u	u	u	u.	•	U	y
	1 USEC	0.1 USEC	10 USEC	1 ÚSEC	0.1 USEC	10 U3EC	1 USEC	0.1 USEC	10 USEC	1 USEC
2N328A[C-B]	0,12316		0-26642	0.14428	0	0.0	0.0	0.0	0.0	0.0
2N32BA(E-B)	11.03790	•	0.11969	0.04439		0.0	0 0	0.0	0.0	0.0
21/335 (C-B)	0.50528	0.32989	0.71045	0.59192	2 0	0 0	2 0	5 6) G	
2N3361JAN(C-B)	0.44212	0.17594	1.06567	0.51793		0	0	0	0.0	0
2N336:JAN(F-B)	C•0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.0	0° 3
(Q-))+8+2K2	0.0	0 0	0 0	00	ى ت	000	ء د د د	90	0 6	و د د
2N3736(C-8)	90	000	0	000	٥ د	20	200	0	0	
2N3736(E-B)	0.0	0	ុ	0.0	0-0	0.0	0.0	0.0	0.0	0.0
2N930 (C-B)	C-23369	О.	0.53284	0.27376	C (0.0	5 6	0.0	0.0	0.0
2K930 (E-8)	0-16946	75	0.28418	0.22197	0-11634		2 C	200	3 C	90
	0.07895	0.02423	0.26642		0.02234	0	0	9 0		0
2N290716-8)	0-0	٩.	0.0	ء -	7	0-0	0.00 0.0000 0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.	0.0	0 0	0-0
2N2907A(E-B)	r c	0.0	0,0	0 0	0 0	0 0	0.0	9.0	0 1	0
2N2222A(C+B)	ء د			0.0	0	0	000			0
	1.67616		8.60734	1.96356	32684	0.0	0.0	0.0	0.0	0.0
F 5911 -3465	0,0	0	0.0	0.0	0 0	0 0	0.0	0	0.0	ဗ္
91011				9 0		0	0	000		
189148	1.11458	0 187	1.17537	1.30570		2	0	3	0.0	0
1N 752A	0.80529	0.94843	1.10563	0.94337	•	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0-0	0	0.0	0,0	ء د د	0.0	0.0
INSUZOBEJAN	20 - 63 - C	**O*O*O**	20286-04	20120-45	#1961°C7	2 5	0 3	9 9	0 0	90
1 N 3 9 9 5 A	7.86338	4.32884	13.98406	9-21174	3,98250	0	0	0	0.0	0
	38.91898	٠.	-268	45.59254	19.72691	0.0	ŋ • 0	o • 0	0.0	0-0
144141	7.98338	4.39850	208	ů.	4.04655	0.0	0.0	o• 0	0.0	0.0
1002	6611139	1.16329	•		1.50	; c) (0.0	96.10
-) C	20,0) a	7	0.0	0	0	0.00274	0.00205
2N33754C-81	0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.02962	0.01990
2N3375(F-B)	٠,	U•1	Ç• (0.0	7	0.0	0	7 •0	0.01363	0 -00 8 75
-	o '	0 :	0,	ے د	င္ (ဝ :	0	0 •0	0 0	0.00604	0.00671
2N1490:JAN(E-B)) (7 G		T 6			200	0.01130	0.01100
2N3504(E-6)	3 7	٥ ٠) (°	000	ر -	0.0		0	0-12772	0.18822
2H2894(C-B1	0.0	0.0	0.0	0.0	0.0	0-0	0.0	0.0	0.02534	0.03040
2H2B94(E-B)) • t	o •		o (و د د	0.0	ာ့ မ	0.0	0.02172	0.01155
2N58294(C-8)	0	0 7	o -	<u>ه</u> د	o :	5 c	ດ	۵ د د	0.01955	0.01860
2N301313000	. q	0	- J	000	0	0.0	0	000	0.0077	0.91277
2N3013: JAN (E-B)	6.	a • 0					0	0.0	0-03620	0.01915
CA3018(C-B)	0.06316	0.03519	0.10301	0.07399	0.03237	0.0	0.0	0.0	0.01260	<u>o</u>

		3 10 10		9	c	•	ć	•	4	6
SM0526517(C-B)	0.00 to 0.00	90	- C- C	0.0	-	0	9 0	0	0.0	
SMB5265176E-91	0.0	0	0.0	0.0		0.0	0.0	0.0	0-0	9
2816131JAN1(-B)	7.40344	0.05978	7.32462	2.91335	0.60698	0.0	0	.	1.14039	76976-0
2M1485138M(C-R)	10 0 0	T ()		0.0	776.10		90	0	0.26833	0-14142
2N14851JAN(E-B)	0.0	0.0	0.0	0.0	0.0	0.0	ر د	0.0	1.18630	3.86229
2h3439f(-B)	4		0 0	0.0	0.0	0.0	ۍ ن	0.0	0.00652	0.00591
2#3439(E-B)	0.0	C 0 0	0.0	0.0	0.0	0 0	2 c	200	0-11730	0-13570
2M7061JAN(E-8)	0.0	0.0	0.0	0.0)))	900	0.00000	#1#10°0
18-69-6735	(* * * * * * * * * * * * * * * * * * *	. o	0.0	0.0	0	0.0	0.0	0.0	0.0	0-0
182580	0-0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.05216	0.90441
1875145JAN 1446627-148	5.92122	1 21955	3.19701	6.93655	9.67378	0.0	0 3	0.0	6606:10	1.36789
1829418:JAN	7.696.5	1.04.04	5,32836	3.50712	1.51746	0	0	0		0.69161
18 302 58 : JAN	13.26353	23.09212	7.45970	15.53787	21.24437	C) ()	0	0.91231	3.04400
M01-354	0.0	0.0	0.0	0.0	0.0	0-0	0 0	0.0	0.0	0.0
IN 746A: JA!!	47.36977	\$3.4.2088	34.63432	55.49240	58.34615	o• o	0.0	0.0	4.23573	10.94316
18645 : JAN	1.37372	0.6 7008	6.66945	-6043	0-61647	0.0	o :	0.0	0.01456	0.31735
THE TO SEPTICAL	0,0	0 0	ဝ ပ	0 0	9,0	٠ د د	ှ (0,0	E # 6 30 ° C	0-01824
181/31A7JAR	0.0	0.0	9 0	9 6	9 0	0.484.00	0-0	0-0		5 6 6 6
254:4 A(F-B)	1.884.24	0, 19243	0	•	0	0.74204	0.56421	0.29024	0	0
2N2E7A(C-8;	0.05955	0.01272	0.0	0.0	0	0.06116	0.03600	0.01919	0.0	0.0
2N257A(E-B)	1.05664	0.01555	o• 0	0.0	0.0	0.04201	0.03627	0.02346	0.0	0.0
24526 (C-8)	96739	0.31154	0.0	0.0	0.0	0.61837	0.60451	6699	0.0	0
2N526(E-B)	1.22109	0.36654 0.04743	0 0	9 0	0 0	0.76107	0.77915	0.55288	5 5	9 0
247.95.A1C-9.3	0.40529	0.18969			. 0	0.61540	0.51384	2861		
2H396A:E-E)	0.0	0.0	0.0	0.0	0.0	0.0	0	0	0.0	0
2K42B#8JAN (C-B)	1.64215	0.46134	0.0	0.0	0.0	1.21296	1 -04783	69969-0	0.0	0.0
2N420 MEJAN (E-B)	0.0	0.0	o•0	0.0	٥٠,	0.3	o,		0.0	0
2N393 EJAN (C-B)	29.775 27	16-02310	ع د د	0.0	0 0	9.17362	18.99904	24.16864	0.0	0
245935JAR(E-6)	0.0	0.0	: C	0 0	7 6	0.0	0.0	0-0	90	
					5		7		0.0	9
24705 :JANIC-B)	0.69674	0.03299	0	0	0	0.05565	0.06045	0.04976	0	9 0
2N 705 : JAK ! E-B }	0-0	0.	0.0	0.0	٥• د	٥.	ې		0.0	0
2N466M2JAN(C-B)	5.05277	1.53%8	0.0	0.0	0.0	3.35347	3.22408	2.32209	0.0	0.0
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	200	2 0		90	0		9 0			200
14277:3AN	0.21316	0.04742	0.0	0.0	0	0-18729	0.13602	0.07153	0.0	0.0
MS1640	0-00495	.0013	0.0	o•0	o•0		0.00443	0.00207	0.0	0.0
)3\$n 1°C	H 10 USEC	H 1 USEC	H 0.1 USEC	1 19 USEC	1 1 USEC	I Jel USEC	JO USEC	J J USEC	J 0-1 USEC
2N328A(L-6)	ر. رو وي	o • o	0 0 0 0	ם ה ה	0.04195	0.04074	0.01422	000	0.0	000
2N335(C-B)	7	10	ر د د د د د د د د د د د د د د د د د د د	30	0.24858	C-16713	0.08127	30	0.0	0.0
2N336 FJANIC-B)	9 0	000	٥. د د	000	0.37287	0.15624	0.04334	90	0	0.0

								,		,
ZN336 8JANTE-6 3	÷ (9	0.0	0	000 800	0.23398	16601-0	9.0	9 0	
10-11-04-7WZ) () c	200		101120	100100	10000			C
/ P-100 P-10) c	ء د د	200	200	14404	04417	10000			0
AR1734(6-1)) c	2		9 6	0.41014	0-15482	0.04795		0,0	0
28430 47-87	, C	0.0	0,0	200	0.18644	0.07730	0.02438	0.0	0.0	0
2890 - (8-8)	୍ଦ	0.0	0	0	0.09943	0.06267	0.03115	0.0	0.0	0.0
2N2+91(C-B)	0.0	0.0	o. C	0.0	0.05179	0.03670	0.00113	0.0	0.0	0
2N2481(E-3)	5°	0.0	0.0	0.0	0.09322	0.02611	0.00598	0.0	0.0	0
242907A (C-S)	0 c	0 0	۵ د د	0.0	0.09322	0.04152	0.01371			9 6
28222245C_81			200		0.11932	725000	0.01788		0-0	9
2022224(F-B)		0.0	0	0	0.14915	0-08461	0.03251	•	0	0
	C	0	0	0.0	3.01166	0.55441	0.00752	0.0	0.0	0*0
F 5911 -3465	0	0	0	0	0.0	0.0	0.0	0.0	0.0	0
14016	0.0	0.0	5.0	0.0	0.0	0.0	0.0	0.0	0.0	9
INZINE	0.0	0.0	0.0	o•0	0.0	0-0	0.0	0.0	0.0	0
119144	0.0	0.0	0.0	0.0	0.41126	0.36866	0.25098	0.0	0	0
1H752A	0.0	0.0	0	0	0.38686	0.26636	5	D. (D. 0	0
	ى 0	ت ن د	<u>ن</u> د	0.0	0.0	0-0	0.0	0.0	2 6	2 c
183026612AN	0 0	ာ ပိ	0,0	0.0	31.00%	10.83380		2 0	9 0	•
143011	2 6	7,0	2 6	9 0	707007	16124-0	1 04443	•	•	
LUSTYDA))	200	2 0	•	4 33449	740047	1 00001	•	•	
17 50 · 00	2 0		9	0	4-67163	,	64787°			9 0
1002	3 6			2 2	1-31487	0.69837	0.28658	200	0	0
24245715-R1	0.04143) c		0	0-0	0.0		0	0.0
282357(F-6)	0.00284	200	0	20	20	200	0		0	0
28357510-83	0.0:135	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
243375(E-E)	0.00320	0.0	0.0	0.0	Ǖ0	2.0	0.0	0	0.0	0-0
2N14901JAN(C-B)	C 203648	0.0	0.0	o•0	6.0	0.0	0.0	0.0	0.0	0.0
2K14901JANEE-31	0.01203	0.0	0.0	J.0	٥ د.	0.0	0.0	0.0	0.0	0.0
2N3584[C-B]	0 0 3331	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N3584(F-D)	6-27755	0.0	<u>.</u>	3 .	Ç• .	o•	0.0	3 6	0.0	0
2N2894(C-B)	C 20 0 0	٥٠	0	<u>.</u> 0	0	0	0.0	0.0	0.0	0
2N20944E-8%		0.0	0.0	0.0	0 0	0	9	0.0	000	000
2N5B291(-0.1)		٠ •	2 .) (2 7	9 6		2 0	•	•
ZMSBZ9(1-6)	50.00.0	•	ָרָ קילי	200		200	Ç (200		2 9
CHACLES CARLES	26100		2 7		, c		200	2 5	200	
	0000		0-0	0.0	9 0	0.0	0	0	0.0	0
(A3010(E-0)	0.00509	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
SMB 5245171(-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
SHB526517(E-B)	0.0	0.0	٥. د	0.0	6• ~	0-0	D• C	0.0	0.0	0.0
2h16131JAN1C-B}	0.27755	0.0	0.0	0-0	0	0.0	0.0	0.0	0.0	0,0
2N16138JAN(1-8)	0.04505	o .	ن نور نور	ت ت ا	ن ق	0	D (0	0 0	0.0
•	66693	0.0	0.0	۵ و	0,0	0.0	0 0	0	0.0	0.0
	11.13000	ه د	2 0	2 6	9 6	•	9 0	200	9 0	
2K343911-4]	5400°0) C) () c	9 0) c		• c	> c	. 5
1	19100		` c	9 6				9 6		
SHIPOAR CANER TO S	45110			2) c		200			
	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3N2580	0.90737	J. J.	0.0	0.0	· • •	0.0	0.0	0.0	0.0	0.0
1N751At JAN	4.42344	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1 N 4 B 5 B 2 JAN	.555	0.0	7.0	7.0	ر و ق	0.0	ر• َ	ۍ 0	0.0	0.0
	0.69387	0.0	0.0	o :	0 °	0 0	0,0	0.0	o. •	0.0
1836258153418	9-71422) c	ာ့ င က င) c	ရ င ာ င	ے د غ د	ء د د	٥ ر و د) () c
F01054	0.0) c) C	9 0	ر د د		2			9 0
PE7-191-8-	•	•	?	•	•	?	•	•	•)

h VALUE FOR RELATIONSHIFE K=P+T++(-N) DERIVEJ FROM EXPERIMENTAL DANAGE LATA FOR TIME INTERVALS INDICATED

N K R 10-1 USEC 1-,1 USEC 10-,1 USEC

.422	0.26144	.588	.349	.363	.475	. 337	.514	208	.364	.389	.578	9.,	234	414	.158	418	.500	3	•	8
301		740		590	٦.	362	5 2 2 8	~	·	3.38674		٠ ٠	0.24715		0.14930	4131J	٦,			.3748
1.41497	0.24988	0.6:206	0.34242	1.36798	C.20412	0.3951	0.50515	0.21388	0.36515	0.39211	0.57403		.2218	4232	.1678	474	.5282	0.395	0.22724	.285
2N328A((-B)	1	3510	24335 (E-B)	3623	2N336 2 JAN (E - B)	9-33515	Ì	73616-8	73616-8	31(0-0)	2N930 (E-8)	-	481 (E	97.7A	90 7A CE	222A	222A1E	ě	Ξ	

INZINE	2596	.23	0.24504
	•	"	6677
PC:15	4227		360
183026B:JAN	ē	Õ	000
h3611	o,	7.	2
1N3995A	1.000	0000-1	1.0000
* 1	3000	1.1000	00000
1002	יים מיים ו	-1-00000	000
2	1107	. 150	1928
N20571E	٠,	949	464
243375(F-B)	2017	, ,	3761
	.5166	7	500
KI 49 CEJAN CE-	4650	.53	2000
2N3584((-B)		23	200
	5520	53	542
150941E	1995	=	161
)16285H	4523	4	446
N582916-6)	3	, .	
1301384 1301384	-	212	707
A3014 (C-B)	.5376	5051	.521
9010E	9446	3424	Ę.
	2670	1404	2450
16135.46K	176	1879	1705
KI & I 3 F JAN (E	327	3435	3354
=	.1962	11890	.1926
N14852JANEE	Č.	0000	0000
343916	431	100	56.25
47045JAN(C-8	783	7360	7606
H7:16 2 JANCE -	.4227	4437	4332
R-69-673	0000-	1.0000	0000
N258C	0000	0000	0000
4 />14 F	0.63849	0.66254	0.65051
129918:3	0000	0000	2000
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1849N	4440.	2 * *	0.2559
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3000	1	9 6	
2N396A(E-B)	1	. 23	77
N428 M		2	196.
N4.28ME.		60.	160
2N3931JANIC-01	7.56427	0.44.0	0.52718
7372	•	ė	000

0.72869 0.60372 0.29251 0.23702 0.08115 0.65938 0.10780	
0.70405 0.64235 0.64235 0.25964 0.25964 0.07086 0.42597 0.64261	
0.75333 0.264C0 0.264C0 0.26324 0.26324 0.263145 0.47712 0.10914	
2NSC1 AZ JANÍC - B) 2NSC1 AZ JANÍC - B) 2NTOS Z JANÍC - B) 3NTOS Z JANÍC - B)	

ARITHMETIC HEAN VALUES FUR QUANTITIES A THROUGH J FUR PULSE DURATIONS OF 10. 1. AND 9.1 USEC

0 16E+ '5	0 20F + 05		0.666+34	416-04		1) . 66E + 14	704 907 O	1011011	0 - 146 + 35		0 . 10E +04	6	C)+367* Ú	404.400	101010
0.356+14	704 346 0	1000000	-25E+04	70131	******	E043067		*0+ 3/ 1* 0	. 4AF+04		0.476+03		-32E+14	704 356 0	0.335.00
2. 1.1F + 16.		60+366-0	115 006		3.345.03	1. 1.06 + 14		E0+3E6-0	20.433.0	10 1 1 C	F0434 0	70.36	1.566+13		70+4K-1-0

POWER TO DAMAGE EQUATION CUEFFICIENTS FOR POPULATIONS REFINED BY A THROUGH J

-1 -1 • F K I T • •

ж Э	0.136E +13 0.527E +02 0.354E +02 0.152E +03 0.45E +03 0.164E +03 0.327E +03 0.366E +03
K 2	0.258E-01 0.258E-01 0.225E-01 0.309E-00 0.103E-01 0.308E-01 0.308E-01 0.308E-01
K 1	0.1168-03 0.1168-02 0.1168-02 0.5588-03 0.15588-03 0.4038-04 0.5138-04

	CENS FRHUDEL BASED UN E. SH DON E. S	APEKINENIAL S	EXPERIMENTAL PARAMETERS Frs	130DK = N	BASED ON	EXPERIMENTAL	PARANC ICES	ARD. BREKE	EXPERITE DATA PARAMETERS AND BEENE DATA NESSENS.
		٠.	J	£	E	r	æ	z	2
	10 USEC	1 0860	9.1 USEC	10 USEC	1 USEC	0.1 USEC	10 USEC	1 USEC	0-1 USEC
N328A(C-B)	0.01958	0.01613	0.01371	7.557	0.06214	3.05291	.07557	0.06214	0.05291
-	9	0.0	0.0	0.03625	0.04849		52980°0	0.04849	0.02876
M335(F-8)	49	0.0	1116	0.21587	0-15020	0-10796	0.21587	0.15020	0.10794
183362JAR(C-B)	0.14596	0.10771		0.0	2		14596	0.10771	0.07786
4	9		0.0	0.0	0.0	0.0	0.0	0.0	0.0
#5484[C-B]	0 0	0.0	0.0	0.0	0.0	0.0	9	0.0	0.0
182484(F-B)	0 6	0.0	٠, ٥	0.0	0 0	۵ ٥	0.0	0.0	0.0
M3/30[(-0)	9 6	2 6	0 6) 3 c	- c	2 6		•	2 0
M930(C-B)	1.63581	1.27409		0.45396	0.35413	0.27242	45396	0.35413	0.27242
M930 (E-B)	9	0	0.0	4-68527	5,55653		4.60527	.5545	6.73626
1N24811(-B)	0.15579	0.04927	0,01558	0.00773	0,00245	0	0.00773	0.00245	0.00077
	0.0	0.0	0.0	0.45908	0.24198	0.13520	0.45908	0.24198	0.13520
N290 7A (C- B)	: • • • •	D (?	3 (c (- O	ر ر د و	0.0	0.0
M2907A(E-B)	0 1	o (0 0	o :	9 0	o :	a a	9.0	9 0
M2/2/A11-8)	9 6	0.0	200						90
N4384	- - -		? .	0.39298	0-13612	0.05241	0.39298	0-13612	0.05241
5911-3465	0.0	0.0	0.0	0-18267	9		0.18267	0.09749	0.04682
N914	ć. Ĉ•	0.0	J.J.	2-29408	1.39921		2.29408	1.39921	1.04891
N2 1WE			0.0	0.0	0	0.0	0.0	0.0	0.0
14014A	1.20360	0.34341	57017	0.11215	0.18916	5.31407	0.11215	0-18916	0.31407
#752A	71136	1.94828	1,52141	21000	0 = 0 3444 0 = 0	0.0	2/485-0	14464-0	1.52161
N30268: 36N		0-0	0.0	0.90359	0.90302	, ,	0.90359	0.90302	0.90375
5	37	7 • • • •	- -	5867	0.16871		0.59671	0.18671	0.05968
N3495A	0.0	0.0	0	1.00000	1.00018	_	1.00000	1.0001	1.00018
IN 3016B	חייח	a-0	0.0	1.77979		1.70011	1.77979	1.77867	1.78011
N4141	0.0	0.0	0.0	1.39781	1.39693	1.39806	1.39701	1.39693	1.39806
	ن (د د	က္ (၁	ر د د	0.11971	7-11964	0.11973	17411.0	0-11964	0.11973
M2857((-8)	ם פר	0.0	o -		9 9	9 0		90	9.0
N3375(C-B)	0	0	0	0	0	0.0	0	0.0	0.0
N3375(E-E)		(•0	r•0	0.0	- T	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0-0	0.0	0.0	0.0	0.0	0.0
MI4901JAN(E-B)	ر ن ک	o•0	0.0	0	0	0	0.0	0-0	0.0
143284 (C-E)	၁ (0.0	0.0	0. 0	0.0	0.0	0.0	0.0	0 (
N3584(f-0)	Q () (• ()	30	0	و	0,0	0.0	0,0
M2894 (C-B)	0 0	0	0 0	0	90	9 6	0 0	9 0	9 6
M.5874(T-8)		0.0	, 0		0	90	9 0	90	
25520 (F-B)	, c	(0		0-0	0	0.0	0	0	0-0
•	0.0	0.0	0.0	0.0	0.0	0.0	0	0	0.0
N3013: TAN [E-B]		0•0	0 • ∙0	o• c	0 0	0	0.0	0.0	0.0
A3018(C-6)	3.27550	3.57206	3.61499	0.0	o c	0.0	3.27550	3.57206	3.61495
M8526517(C-8)	֓֞֝֜֝֜֜֝֜֜֝֓֜֜֝֓֓֓֓֜֝֓֓֓֓֓֜֜֜֓֓֓֓֓֓֓֓֜֜֜֓֓֓֡֓֜֜֜֓֓֡֓֡֓֜֜֡֓֡֓֡֓֜֡֓֡֓֡֓֡֡֡֓֡֡֓	0-0	0-0		0	9 0	0.0	0-10	0°C
HB5265176E-B)	υ •	2	10	0.0	0.0	0.0	9	0.0	0.0

2W14131 14 14 14 14 14 14 14 14 14 14 14 14 14	14 70464	4 07704	2 34.3.78	10440 7	26628	1 12086	10000	3 34630	1 12004
7	0.0	0.0		4.91271	3.3115.6	2.30324	4.9127	3,30155	7.30324
241445; (AMIC-R)	0-0		9	0	0		0-0	0	
2814852.1AM(F-R)	0		- C		9 5	0-0	7	0-0	0-0
283434(C-8)	5	0.0	0	0.0	0-0	0,0	0	0	0
2N3439(F-B)	0	0-0))	0.0		0-0	5	0	0
2N706 : JAN! C-8)	0.36441	0.69971	1-21057	0	0	0.0	0.36441	0.69971	1.21057
2N706 EJANIE - B)	0.0	0.0		0.0		0.0	0.0	0.0	0.0
18-59-6735	0.0	0.0	0.0	<u>ي</u> 0	0.0	0.0	0.0	0.0	0.0
182580	0.0	0.0	· · ·	0.0		J•0	0.0	0.0	0.1
1N751 A: JAN	0.0	0.0	0.0	0.22793	0.75088	2.42220	0.22793	0.75088	2.42220
INCASSBEJAN	0.0	0.0	ن.	0.51760	0.71207	1.03539	51760	10211-0	1.03539
IN2991BIJAN	ن 0	0.0	ت 0	1.12948	1.12877	1.12968	1.12948	1.12077	1.12968
1. 502592JAR	J•0	0.0	· • ·	59192	1.87199	5.92027	.59192	1.87199	5.92027
MOTOSA	0.0	0.0	0.0	0-0	0.0	0.0	0.0	0-0	0.0
PPTC . C.JAN	0.0	o•0	0.0	2-39030	5.81498	14,14205	2,39030	5-81498	14.14204
11:545 J.N.	ပ္	0.0	0.0	0.43924	0.16114	0.14278	0.43924	0.16114	0.14278
MALIANEC MI	0.0	۰,•۲	. · ·	Е.C	0.0	0.0	3.0	0.0	6.0
IN1 IND	ئ د د	0.0	o•0	0.0	0.0	0.0	0,0	0.0	0.0
*N4034(C-F)	4.12507	1.73944	3.7967.6	0.37951	0.160/3	0.07275	0.37951	0.16003	2.01275
WACARIE - D.)	9	0.0	0.0	0.50679	0.21575	0.08529	C.50679	0.21575	0.00529
2×291415 - 61	ر. ق	0 * 0	÷.	0.11376	0.03958	0.01536	11376	0.03958	0.01534
• •	O.	0-0	0.0	0.11209	0.05317	0.02643	0.11209	0.05317	0.02643
2052c (C J)	.18687	1-19702	71507	0.17202	0.09416	0.05625	0.17202	0.09416	0.05425
2N525(E-8,	<u>-</u>	ئ. 0	0.0	0.26355	0.15107	0.08237	0.26355	0.15107	0.08237
. 16 10	•		7.	J.04354	0.11457	0.00527	0.14354	0-01450	0.00527
19308A(C-1)	4.18039	1.95437	0.83623	0.0	0,0	0.0	4.18039	1.95437	0.43623
1330FF F		က ်	0	0.0	٠ • •	0	0	0.0	7.0
2. 625% 6 JAF . C. 13	6.1797}	5.94903	1.52702	0° 0	0.0	0.0	6.17971	2.98903	1.52702
	-	?		ب ا ا	~ ·) · O	000	0.0	0.0
2N35 3N1C 31	19 4 5 4 9 1	1 506 2	11112.77	0.0	0.0	0.0	19952-39	79.15062	77.37111
343635 THE P. P. P.		۔ د	3•1	D.C	0.0	0.0	ت د	0.0	0.0
	ر. ج: ع	6970 ;	2.40732	0.0	0.0	0.0	0.83962	1.50449	2.40132
19-4 44 10177		•))	0	 	ڻ•ر • •	0.0	0
28.105 a 2013	Y 9 0 1	7.49514	0.31318	0.0	0.0	0	0.81412	0.49514	0.31310
		5 C	7.0	7 (200	٠ ٠ ٠	200	0.0	0.0
	•	3 6 6 7	1.04625	٠ •	o .	o.	9.2256	2.97450	1.04623
			~ (3.0		200	ာ (•	D (
		3	o .	.	C .	o .	2	?	•
10104296 1X1 -81	•			٥ •	ن. 0•	0.0	0.0		0.0
182771.175	ت. ن	ن ^ي	0.0	0.96461	0.39223	0.15850	0.96461	0.39223	0.15050
	Ç	• 1	1.0	0.17594	0.04121	0.02200	0.17594	0.06121	0.62200
	C.10/ Fet 2								
0.5246+4	11,774.								
	10+3185								
	5 37 E 3								
	C. (141.).								
0.564E+10	E(♦ 7 % - 8 €								

ON HIGH POWER OR LOW POWER RATING FOR ALL DEVICES ON HIGH POWER UR LOW POWER RATING FOR ALL DEVICES KA DAMAGE CONSTANT BASED KA DAMAGE CONSTANT BASED DE EXPERIMENTAL PUNER TO CHACLE, FOR THE PARKERS OF THE CONTROL OF THE PARKERS OF THE CONTROL OF THE PARKERS OF THE CONTROL OF THE PARKERS OF THE STATE AS PEXCEPT FOR SILICON DEVICES WELL SAME AS DECEPT FOR GERMANUM DEVICES OF THE TESAME AS DECEPT FOR GERMANUM DEVICES OF THE CONTROL OF THE

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	0	0	0	•	•	G.	9	n	o.
	10 USEC	1 USEC	0.1 USEC	10 USEC	1 USEC	0-3 ESEC	10 USEC) USEC), u usec
2N328A(C-B)	0.125	0.130	0.134	0.125	0.103	0.080	151.0	0.125	0.134
2H326A(E-6)	٠.	040.0	0.037	950.0	0.032	0.018	950.0	0.036	0.029
2H335 (C-B)	∹	0.199	0.298	0.125	0.158	0.186	6-121	0-192	0.267
2N335(E-B)	٠:	0-110	0.00	0.125	180.0	60000	7.10		0.00
2N336 5JAN(C-6)	-	0.174	0.159 	967	0.139		- A	0.26	265.0
7M3643AM1E-87	• `	0.115	050-0	0.263	0.091	0.031	255.0	C-111	9500
2N2484(F-B)	١٩	0.120	0.159	760-0	560.0	0.100	1.041	0.115	0.153
2N3736(C-B)	~	0.179	0.114	0.275	0.143	0.072	0.26b	0.173	0.110
2N3736(E-B)	649	0.636	C. 585	0.689	10 M	0.369	75.7°C	0.613	0.564
2M93U(C-B)	; -	# 0 T = 0	0 228			0.144	1000	991 3	0.220
2N2481(C-8)	: 0	0.025	0.010	0.063	0.020	900.0	0.0	0.0	0.010
282481(E-B)	=	0.075	0.053	0-113	650.0	0.033	0.109	0	0.051
2N2907A (C-B)	7	0.132	0.134	0.175	0.105	0.085	0.121	0.127	0.129
2N2977A(E-B)	۳,	C.194	0-109	0.332	0-154	690.0	0.320	(c. 3 6 :	9-105
2N2222A(C-B)	~!	0 -212	0.216	002.0	0.166	0.138	0,193	407-0	012°L
2M2222A(E-B)	4	0.336	0.135	067-0	0.220	20.0	445.0	0.267	02, 0
F 50 11 - 344 5	3		0.0	9	0	200	0	0	0,0
1 NE 16	0.424	0.325	0.307	0.424	0.258	0.194	776.0	0.590	0.37
14214E	-	ت ن	0.00	0.0	0° '1	0.0	0.0	0	0.0
1 N9 1 4 A	9	0.199	0.417	760-0	0-156	0-263	0.091	0.192	207-0
1N752A	ή.	148 0	2-282	0.520	0.673	1.440	105.0	1100	7.200
PC135	1	641.0	0.158	****	671.0	0.100	4.581	247.4	1 + 1 + 2 P
18 37 200 2 JAR 1836 1 1	: •	0 34.0	771-0		0.247	100.0	000	0.322	60.00
1 M 3 9 9 5 A	. 3	0	0	0	0.0	0.0	0	0.0	3.0
1N3016B	•	4.450	6.236	3.935	3.933	3.934	3.503	4.467	5.55?
14141	4	3 . (4.6	3.837	2.422	2.42)	2.452	2.156	2.712	3.416
7001	⇉	5.277	6.647	4.195	4.192	4-196	4.045	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.4.9
2N2857(C-D)	9	0,00	0.00		260.0	7000	6000		^[170
ZMZ837(E-8)	1.1.5	0.00		141.0	600°C	480.0	0.135	101-0	0.077
2N3375(E-B)	9	0.053	0.062	0.010	0.042	0.039	0.062	0.047	0.054
2N14905JANIC-BI	~	C.277	1.336	0.212	0.220	0.212	9.169	0-247	0.299
2N14905JANIE-B)	٠,	0.458	0.624	968.0	0.364	0.394	0.350	0.408	0.555
283284(C-01	٦.	V 20.00	16040	387.0	667.0	8000	0 . 13		0.07
20122041CT01		0.126			907-0	0.104	0.065	6-120	0 - 163
(P-3)9682W2	9	0.047	0.030	0.075	0.036	0.019	0.072	0.04	0.029
2N5 829(C.4)	5	2.042	740°C	0.038	41000	0.029	0.036	0.041	0.045
2N5029(E-B)	٩,	0.025	0.022	0.027	0.026	0.014	0.026	0.024	0.021
2N3013EJAN (C-B)	3	0.052	3-099	0.027	0.042	0.083	970"0	0.050	960-0
2N30132JAN1E-B1	7;	0.079	0.052	0.125	0.062	0.033	0,121	0.07	0.050
CA3018(C-E)	ç	0.00	J.763	9E0 0	0.040	2000	\$ 0°0		1.00
	3	6 40.0	7700	6700				9000	• • • •
SHR52451716-8)) 0	• (0.0	0,0	0.0		9 0	9 0	0
2N16138JANIC-81	1.745	۲,	3-175	9.766	4.150	: 8	6.452	5.047	3.061
2N16131JAN (E-B)	20 0° 1	•	97.0	1.002	0.673	0.410	796.0	0.817	0.718
2N14858JAN (C-8)	0.212	.13	0-082	0.212	0.105	ė,	٠	0.118	0.073

	,			,	1	•		•	•
ZM14852JAH (E-B)	00000	3.60	13.910	866.0	7/9-7		668.0	3-619	•
24343714-61	600°0	0000				70000	600-0		.
COLUMN TO THE PORT		200			2000				•
THE LOW THE STATE OF THE	810.0	7,00	260.0	210.0	\$ 0°0		1000		>
ZM F.O. 5 JAR. 17 - 0.1		500	2000		96000	160-0			,
1816916 (37	77.	6,44	0.0 4.1.8	441.4	143	741.4	(6)	26.2	-
18751 45 148	C		25.300	1,502	160.4	15.069	1.469	100-4	7.
	0.626	700-1	1.084	454.0	148.0		704-0	1-045	
IN299381JAN	3.027	3.808	4.797	3.027	3.025	3.028	2-695	3.390	•
1 N 3 U 2 5 B 2 JA N	× 4.0	1.687	6.715	7240	1 .340	4-239	176.0	1.502	•
KD1054	0.0	0		0.0	0.0	0.5	0	0	•
12746 A 5 JAN	16.278	448-64	152,593	16.279	39.603	96.314	15-696	40.00	=
2000 4 CONTRACTOR	0.0.0	001.0	710-1	16100	760	0.272	0.027	0.107	•
1217312412	0.242	0.241	0.273	0.242	0.191	0.173	0.216	0.215	, 6
284048(C-B)	0.751	0.399	0.228	0.751	0.317	0.144	0.0	0.0	0.0
2N404A[1-8]	0.651	0.349	0.174	0.651	775-0	0.110	0•0	0.0	•
2N297A(C-B)	0.605	0 -265	0.130	509-0	0.211	0.082	0.0	0	
2N297A(F-B)	9750	0 -253	0.158	924.0	102.0	0.100	9 6	0 0	
28526 (C-B)	********	200	225-0	418.0		997-0	9 9	9 6	, .
ZM3Z6 (E-6)	700-1	671.0		1.002	040	\$16-0		9 6	, ,
25396Aff -B.1	0.720	424.0	0.228	0.720	0.337	0-144	0	0.0	
28396411-81	4. 3° 0	0.511	0.347	0.614	9340	0.219	0.0	0	. •
2N428# 3AK (C-B)	1.064	0.648	0.417	1.064	0.515	0.263	0.0	0-0	•
2N428M3JAN (E-B)	1.377	969-0	0.332	1.377	0.554	0.210	0 0	0.0	
2K393 8 JAN (C-B)	1.078	2.742	3.373	1.878	2.178	2.129	0.0	0	
28399 table ()	0.207	0 .399	6642	2020	0.317		D 1	2 0	,
28501452ARIC+01				1000	460-0	460.0	90		.
24.704.4.44.6.4.5.4.5.4.5.4.5.4.5.4.5.4.5.4.5	940	0 033		340.0	0.00	0.010	6	0.0	
AND STANSON STANSON	0.023	910.0	0.012	0.023	0.013	0.00	0	0	
2N446HIJAK (C-B)	2.942	1.994	1,349	2.943	1.584	0.877	0.0	0.0	0
2N466 MIJAN (E-B)	100-7		0.923	£ 000 5	1.564	0.582	0.0	000	-
2410424AJAN (C -61	0.151	0.191	0.192	0.151	0.144	0.121	90	9	
24104784JRW(t -67		200	0.00	*OT *O	0 136	777.0			, c
116.7.7.5.			0.0		0.0	0.0	0	9	. •
			•	3	2	3		3	
	•								
	•	4	*	~	~	~	-	-	-
	13 USEC	1 USEC	0.1 USEC	10 USEC	1 USEC	0.1 USEC	10 USEC	1 USEC	0.1 USEC
	•		•	Ġ	ć	ć	Ġ	•	•
2N328A(C-1)	70	160.0	20°0) - - -) (2	0	
2N335 (C-6)	۳,	0.153	0.101	0	0.0	0	0	0.0	0.0
24335 (E-B)	∹	790.0	0,060	o.	C. 5	3 (د. ه	0 0	0
2N336 EJAN(C-B)	٠, ١	0.134	0.097	ت د د) ; o c	90	0 0	9 0	9 0
2N2484(C-B)	0.254	8000	0.030	0	0	0.0	0	0	0
2N2484(E-B)	0,	260-0	160.0	0.0	0	٥ •	0	0	0.0
ZN3736(C-B)	0.266	0.137	A 0 0 0	o••o	2	2) 5	2) · O

2N3736(E-B)	4	764.0	0.356	0	0	0	0.0	0	0
(G-3) 0E6M2	٦,	0.141	0.100	o .	0,0	0	0.0	20	2
2N930 (E-B)	260-0	0.115	0.139	0.0	0,0	o.	D (0,0	•
2N24811(-9)	ç	6100	90000	0	ن دور) •	<u>ء</u>	0	3
2M2481(E-B)	7	0.057	0-035	0.0	0	0	0.0	0	0
2N2907A (C-B)	7	0.101	2000	0	0,0	0.0	0.0	0	0
242907A(E-B)	0.320	0.149	990-0	0	o :	o *	0.0	0.0	•
2N2222A(C-B)	7	9-162	0.133	2 (. · ·		5 (3 (9
ZNZ ZZ ZA (E-B)	142-0	267-0	247.0	ء د د) (2 5	90	•	200
184201 F. Co. 11 - 34.45	ů.				2) c			90
1 37 11 - 54 55 1 ME 16	- 117	0.230	3.173		0	0	0	0.0	0,0
102146	9	0.0	0.0	0	ပ္	0.0	0.0	0	0.0
1M914A	16000	0.153	3.254	0.0	0.0	0.0	0.0	0.0	0.0
1117524	0.501	0.649	1.389	0.0	0.0	0.0	0.0	0.0	0.0
PC115	0.137	0.115	0.089	0°0	0.0	0.0	0.0	0	0.0
1 N 3 0 2 6 B : JA N	4.501	4.579	4.582	0	0	0.0	0.0	0	0
183611		0.256	1000	50	5 c	3 6	9 0	90	2 0
1434954 113	2 E	2 6	3	ء د د	9.0	•	9 0	2 6	•
3830188	3,503	3.501	3.504	200	200	2 6	, c	2 0	
1002	4-045	6.043	940-7						
2N2857(C-8.)	0.075	0.031	0.072	0	0	0	0	0	0
24/2457(E-8)	005	0.00	500.0	0.0	0.0	0	0.0	0.0	0.0
2N3375 (C-B)	0.135	0.085	0.049	0.0	0.0	0.0	0,0	0.0	0.0
2N3375(E-B]	790"	960.0	3.035	0.0	0.0	0.0	0.0	0.0	0.0
2N1490:JAN1C-B1	641 641 7 17	0.196	0.189	0.0	0.0	0.0	0.0	0.0	0.0
ZMI49() CJAN(E-B)	066.	455.0	0.350	0.0	0.0	0.0	0.0	0.0	0.0
2N3584 (C-8)	0.032	6	0.032	0.0	ũ°0	0.0	0-0	0.0	9
2N3504(E-0)	Services of the objective of the objective of objective of the objective of the objective o	=	0.270	0-0	0	0	0	0	0.0
2N2894(C-B)	0.0	ę.	601.0	C	0.0	٥٠,	0.0	o (0.0
2%2494(F-B)	1.072	0.036	0.018	0.0	٠ •	ට (در ۱ 0		0
2N5629(C-0)	96000	Ĝ	9700	0	۵. ۵.	<u>ء</u> د	٠, ۵	200	9 0
2858291F-BJ	4.0	5	510-0	200) c	9 0	200		•
283013:348(C-B)	20.0	5 3		9 6	9 6	9 6		2 6	9
CA20136281C-87	3 E O - O	460.0	0.00					200	
	1.026	3	0.013	0	0	0	0,0	0.0	0.0
SM8526517(C-8)	0.0	9	0.0	0.0	0.0	0.0	0.0	3 0	0.0
SHB526517(E-B)	5	200	0.0	0	0	0.0	0	0.0	0.0
2N1613FJAN(C-81	8 .4 52	Ę,	1.932	0.0	0.0	0.0	U.,U	0 0	0.
2416132JAN(E-B)	996.	• 1 0	0.453	0	0.0	0	0	0	٠
2414651JAN (C-B)	0.189	ę:	950.0	o c	0,0	٠ • •	ပ္င	0 0	•
ZN146553AN(E-6)	7.0 G	1 66. 0	100	2 0	2 0	o -	2.5		•
[B.] 16 C L C L C L C L C L C L C L C L C L C	690	0.00	900		9 0		2 0		9 6
28.706.5.1AM(C-B)	0.017	0.032	0.05	0	0	2	0	9	
2W7.6514M4E-81	140	0 03+	0.030	0	0.0	0.0	0.0	0.0	•
18-69-6735	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	٠
182580	4.581	4.579	4-502	0.0	0.0		0.0	0.0	•
IN751AEJAN	٠,	4.773	15.398	0.0	0.0		0•0	0.0	
1M4.85.81.JAN	70 9 ° (0.031	1-208	0	0		0	0	٠
12299181149	2.695	2.693	2.695	D (٥ •		0,0	0	٠
1 N30258 1 7 M	0.377	1 - 19 3	3.174	0.0	٥ ٥		0 0	٠ •	•
MO1054	0.0	0.0	0.0	50	0,0	9 0	ء د	9 0	9 0
12/40 As JAR	ہ د	101	140.0)))	ş c		2 9	9 6	
1212-0-2845 1212-0-2845-148	7.0.0	5 90 0	0.243	0	0	0	0.0	90	9
141731A:JAN	~	0.170	0.154	0.0	0	0.0	0	0	0
2N4U4AIC-B)		0.0	0.0	718-0	0.434			0.344	

0.219 0.219 0.219 0.219 0.219 0.219 0.219	40000000000000000000000000000000000000		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 nsec	
7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	# 10 USEC	2 2 2 3 3 3 3 5 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6
00 00 00 00 00 00 00 00 00 00 00 00 00	1.116 0.093 0.093 0.093 0.093 1.510 1.510 0.595 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025	v 0.1 USEC	0.4684 0.4684 0.660 0.00
00000000000000000000000000000000000000	0.434 0.046 0.046 0.049 0.049 2.168 2.168 2.168 0.049	J USEC	
	20000000000000000000000000000000000000	10 USEC	00000000000000000000000000000000000000
	MITHEUT MITHEU	u 0-1 USEC	0 - 3 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -
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2 N + 10 + 4 + 11 + 12 2 N 2 9 7 A + 12 + 13 2 N 2 9 7 A + 14 + 15 2 N 2 2 4 (- 16) 2 N 3 2 6 (- 16) 2 N 3 9 6 A + (- 16) 2 N 3 9 6 A + (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A (- 16) 2 N 4 2 8 N 2 A A A A A A A A A A A A A A A A A A	2839352AM6E-B) 288518ATAN(C-B) 288518ATAN(C-B) 288518ATAN(C-B) 287558AAN(C-B) 287568BAAN(C-B) 287568BAAN(C-B) 287668BAAN(C-B)		2N328A(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N338(C-B) 2N348(C-B)

	6	e d	4		2	6		ננניט	976
7/113 1830/48: [48	722.0	1 2 20 5	15.489	9.75	0 76.9	0.170	0000	13.019	13.883
183611	1.725	0.687	0.273	1.725	0.546	0.173	1.546	0.615	0.245
129954	0		0.0	0-0		0.0	0.0	0	0.0
10000 F	76.7	200	1 .	7 4 7 5	6.4	7.47	804	A - 4 2 A	10.415
200000		704	7 2 6 7			104 7	7 1 2 2	41.4	CE 5 . 4
1002	10.45	13.151	16.567	10.455	344.01	10.457	23.804	24.946	37,723
24285765	0.0					0.00	0	0-0	0.0
2N2857(E-B)	0 (9	0.0	0	0	0.0	0	0	0.0
2N3375(C-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0*0
ZN3375(E-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N1490=JAN(C-B)	0.0) *0	0.0	0.0	0.0	C•3	0.0	0-0	0.0
2N1490: JAN(E-B)	ن- 0	0	0.0	0.0	0 0	0.0	0.0	0.0	0.0
2N3564(C-0)	o• 0	0,0	0.0	0.0	0.0	ء د د	0,0	0 0	0 0
ZN3564(F-1)	- c	2 0	200	2 0	2 0	9 6	•		•
19-31-492N2	200	9 6			90	0.0	200		
2N5829(C-B)	0	0	0	0	0	0.0	0	0	0.0
ZN5829(E-B)	2	0.0	0.0	0.0	0.0	0-0	0.0	0-0	0.0
2N3013=JANIC-8)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N3013=JAN(E-81	ာ	o• 0	0.0	0.0	0.0	0.0	0.0	٥ • ٥	0.0
CA3018(C-6)	060.0	0.124	0.158	0.091	660.0	0.100	0.206	0.483	0-360
CASULB(E-B)	79.00	790.0	*CO*O	790-0	A 0 0	0.034	741-0	1.0	0-14
SMB526517(6-0)	9 5) 5	200	200	- c	200	- - -	200	
COLD NALL OF LAC	21.845	13.044	7.913	21.847	10.364	4.94	072-67	20.701	18.017
2816132 IAN 86-81	7-697	2.112		7.497	1.678	1.171	5.6.5	9 OB - 7	4.223
2N1485+JAN(C-0)	0	0.0	0	0	ر د د د	· ·	0	0	0.0
2N1485=JAN(E-B)	0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N3439(C-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N3439(E-B)	0.0	0.0	0°C	0.0	0*0	0.0	0.0	0-0	0-0
2N706 : JANIC -8 J	0.044	0.106	0.230	0.044	1.084	0.145	660° r	0.240	0.524
2N7U6 : JAN(E-B)	٥ ٥	0	0	0	0 -	0.0	င္ -	0.0	0
IR-69-6735	0.0	0 0	0.0	D ((·	0.0	0 0	0 0	0
IN2580	000	0	0 0	0	0.0	0.0	0.0	0 0	0.0
18/5145JAN	3.745	876-61	63.155	5.745	12.33B	29.199	176.8	35,359	143.5/4
	1 2 500	2010.2		1.200	2 744	5 75)	6 163	2740	797.
1029715 - 35 K	100°C	363° /	12.756	200	775	100.8	0.723	2.872	11.432
M01054	0.0	0	0	0.0	2	0.0	0.0)	0.0
1 N746 A : JAN	40.568	124.230	380,305	40.572	96.701	240.042	92,373	282.868	865.946
1 N645 = JAN	7.802	3.603	4.018	7.802	2.862	2.536	17.764	8-203	9.149
IN1202RA:JAN	0 0	0	0.0	0	0	0	0.0	0.0	0.0
INI / 5 IN I AN	0.0	o 0	. · ·	2.0	- (2 (9))	200
24 04 4 C - B 3	1.627	766.0	0.569	1.673	064-0	0.359	0		
287974C-83	1 - 1 50	905-0	0.246	1.150	0.4.0	0.155	0	0	
2N297A(F-B)	508.0	0 .481	301		0.382	0.190	C	n•0	0
2N526 (C-E)	2 -0 28	1.398	1.051	2.029	1.110	0.663	0.0	0	0
2N526 (E-B)	764.5	1.801	1.236	165.5	1.431	0.780	0.0	0° 0	0.0
1N270	0.296	0.124	0.057	0.296	660.0	0.036	0.0	0.0	0.0
2N396A(C-B)	1 - 7 94	1.056	0°269	1.795	0.639	0.359	င္င	0	0.0
CHANGE TO J	200	2.4	0.0	0.0	, c	0.0	9 0	2 0) c
78772277X7	200		0-0	0.0	6000		0.0		
2N393:JAN(C-8)	4.681	6.633	F 0.4 € 7	4.681	5.429	5.307	c.	0	0
2N393:JAN(E-B)	0.0	0	0.0	0.0	0-0	0.0	0.0	0.0	0.0
ZNSO1A=JAN(C-B)	2,0.0	0.136	0.213	0.047	7.084	0.134	0.0	0.0	0.0
2NSG1 ATJAN (E-B)	0.0	0.0	0.0	ر 0 0	0.0	0	0.0	0.0	0.0
ZN705 : JAN(C-6)	0.172	0.093	1.0 16	0.124	5 0 74	140.0	ت• -	ũ•u	o•o

2N705 # JAN(E - B) 2N466M # JAN(C - B) 2N466M # JAN(C - B) 2N1042R A JAN(E - B) 2N1042R A JAN(E - B) 1N277 # JAN	7.34 7.334 0.0 0.0 0.0 0.2	6 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	7.334 7.334 7.334 0.0 0.0	8 3 4 0 0 0 0 0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.036	000000	000000	000000
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24335 (C-a) 2N336 £-B] 2N336 £JAN (C-B) 2N24645(C-B)	11.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 4 F 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	၀၀၀၀ ၀၀	ମୃକ୍ତ୍ର ୧ ୦ ୦୦୯୯				
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2N248 1(E-B) 2N248 1(E-B) 2N2907A(E-B) 2N222A(E-B) 1N4384 F 00:1-3465) 0 3 0 0 0 0 0 0 0					
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9,10403 3,11749 1,60721 0,68983 0,50403 0,24912 0,24912	0.1989 0.17473 0.08650 0.08650 0.096650 0.029650 0.019850 0.01063	6.99276 1.85524 1.08422 0.46422 0.28720 0.28720 0.0999 0.03994 0.01988 0.01988 0.01988 0.01988	1.81741 0.65655 0.33643
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12.93426 5.11189 1.81046 1.32422 0.79595 0.40968	0.21947 0.13266 0.13266 0.09406 0.07960 0.04975 0.04975 0.02633 0.02255 0.01821 0.01227 0.0063	13.11916 2.70573 1.33195 0.60879 0.35780 0.20812 0.05073 0.05073 0.01385 0.01385 0.00135	3.03070 1.7575£ 0.42404
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567 598 598 598 598 598 598 598	0.24538 0.18744 0.18518 0.08175 0.08174 0.03766 0.02726 0.01924 0.01924 0.01924 0.01924 0.00925	14.09522 3.67336 1.47051 0.68876 0.38959 0.22303 0.07118 0.05248 0.05248 0.02122 0.02128 0.02128 0.02128 0.02128	8.11673 0.93952 0.51238
94446		17.24905 4.63029 1.63905 0.71560 0.22322 0.22322 0.05928 0.05928 0.02347 0.02345 0.02345 0.02345 0.00345	12,49399 1,07321 0,5445C
N. N. S. N. D. S. A. W.	4	19 20517 6.49343 0.693889 0.6139889 0.139879 0.139879 0.13982 0.056117 0.056117 0.01548 0.01174 0.01174	14.72355 1.38886 0.54713

0.16572 0.04357 0.02357	23.09212 7.699212 7.69997 1.699109 0.66109 0.12966 0.057316 0.057316 0.057316	19.72691 7.26594 2.41344 1.19563 0.26642 0.10301 0.0439	0.77215 0.51384 0.13402 0.03627	1.18830 0.51452 0.09302 0.09328 0.01860
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0.17679 0.04924 0.02499 U.00292	28.04044 7.86338 4.00081 7.03415 1.31955 0.51344 0.51344 0.18243 0.19243 0.03790 0.03790	25,79674 3,0034 3,19701 1,21396 0,71045 0,28418 0,11989	1.04783 U.56421 U.17128 U.04281	3.06408 0.69161 0.26833 0.10943 0.01927 0.01927 0.01963
0,19952 0,05411 0,02982 U,00631	29.775.27 7.98338 4.10749 2.06919 1.37372 0.58679 0.58679 0.32989 0.056601 0.03912 0.03912	34.63432 9.21174 3.50112 1.30570 0.71.045 0.1426 0.05311	1.23296 (0.abc45) 0.18729 14976	3.8629 0.69387 0.27755 0.11730 0.01331 0.01995
0.21720 0.05683 6.03031 0.01169	38,14102 4,19291 4,19291 2,08635 1,94848 0,355649 0,25692 0,25692 0,25692 0,25692 0,07895 0,07895 0,07895	45.59254 9.32462 3.32462 1.51343 0.87254 0.12556 0.12556 0.01133	2.32209 0.61540 0.25419 (15351	4.23573 0.81456 0.27755 0.015772 0.01390 0.01459
0.2249U 0.07733 0.02031 0.01212	38.91898 4.31837 4.39850 2.11139 1.010555 0.386215 0.38659 0.38659 0.15256 0.08150 0.08742	55.49240 9.35232 3.98250 1.51746 C.93725 C.32684 U.14801 0.07138	3.22408 7.61837 6.2861 7.95565 0.00207	442344 0.85234 0.13033 0.13033 0.02140 0.01473 0.01155
0.23235 0.08945 0.02379 0.01429	47.36977 13.26353 4.73942 2.34714 1.018477 0.39119 0.39642 0.05113 0.05474	58.34615 9.6178 4.04655 1.60528 0.943?7 0.47169 0.16186 0.02234	3.35347 0.64482 0.06482 0.06645 0.06645	9.7442 0.90442 0.31735 0.14093 0.02403 0.01403
0.28519 0.09938 0.03788 0.01705	49.87672 16.42310 5.62277 2.48891 1.146944 1.146944 1.146944 0.293119 0.29697 0.05369	59.62102 13.986.06 5.32836 1.93114 1.06567 0.21793 0.20693	9.1736.2 C.6966.3 D.3566.1 D.061.16	10.94316 0.90337 0.3808.2 0.155.70 0.052.4 0.00534 0.01531
0.28623 0.11264 0.03975 0.01749	50,89406 18,7051 5,13437 2,93392 1,57391 1,16791 0,670266 0,2791 0,02738	69.28662 14.236662 6.560455 1.96356 0.253284 0.22193 0.03237	18.99904 C.74204 C.38149 C.07153 0.011919	11 0 2 3 3 5 0 2 3 3 1 0 2 3 3 5 0 2 5 0 3 5 0 3 5 0 3 5 0 5 0 6 5 0 7 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.33674 0.11926 1.4357 0.02273	63 -42088 21.44208 5.97122 2.99377 1.68701 1.1737 0.64212 0.17594 0.11756 0.011756	90.582U5 15.53767 6.93655 2.13126 1.07020 0.26642 0.0116 0.03699	24.16864).76107 0.46995 0.07153	26-67943 1-14043 1-5551 0-15265 0-03940 0-11824 0-03940

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APPENDIX	

0 0 9 00 ° 0	6.66439 1.53912 0.36107 0.11229	2.64061 0.41126 0.24703 0.14703 0.07708 0.01806 0.00305	0.20914	2.35117 0.34341 0.01958	2.42220 1.39606 1.00016 0.59192 0.24198 0.05968
0.00648	7.03699 1.68500 0.39302 0.11262	3.01166 0.42731 0.26858 0.08127 0.08127 0.06334 0.00564	0.24604	3.27550 0.3641 0.04927	3.30155 1.39921 1.03539 0.59671 0.13612 0.06214
0.00652	7.90835 2.11751 0.42545 0.11678	0.05541 0.55441 0.15982 0.08461 0.06512 0.00598	0.26073	3.36278 0.57017 0.07786	4.68527 1.77867 1.05891 0.63444 0.14278 0.07557
0.00285	8.00845 2.15038 0.45048 0.12763	4.97163 0.25098 0.16406 0.06752 0.06795 0.02709	0.30078 0.03123	3,57206 0,69971 0,10771	4.91271 1.7979 1.12877 0.71277 0.35413 0.08625
0.00509	2.9866 2.54529 1.10728 0.15016	5.28265 0.28206 0.26536 0.09192 0.09113 0.09115 0.0935	0.32083 U.03183	3.61499 0.98166 0.14596	4.98501 1.78011 1.12948 0.7508 0.39298 0.09749
0.00763	9.5828 2.60275 1.26776 0.18341	6.90781 1.00643 0.20658 0.16931 0.09322 0.05321 0.01117	0.38767 0.34318	6.97798 1.21057 15579	5.55653 1.87199 1.90308 0.90302 0.43924 0.18267 0.10796
0.00778 C.00543	19.25011 2.69600 1.27635 0.19257 05390	12.87296 0.8858 0.186866 0.09322 0.09322 0.05541	0.43664 0.0752U	10.08529 1.27609 (2.3560	5.81498 1.13488 0.96398 0.65398 0.18871 0.11215
0.00820	19-25713 2.80296 1.89136 0.19257 U.US615	16.03366 1.31487 0.31781 0.09322 0.04111 0.0674	0.52397	14.49531 1.52161 0.20738 0.01371	5.92027 2.30324 1.35731 0.90375 0.45908 0.11964 0.05129
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4.91271 2.30324 1.39781 1.00018 0.59671 0.13596 0.09749	6.64741 3.04606 1.68690 0.71997 0.6209 0.39686 0.39686 0.25968 0.18782 0.18782 0.1966 0.017986 0.017986	5-14-59 1-44-59 1-44-59 1-44-59 1-44-59 1-44-59 1-46-59 1-4
4.90601 2.35117 1.39800 1.03539 0.83444 0.3544 0.15020 0.15020	6.71535 4.94983 3.13031 1.87818 0.72276 0.43824 0.33817 0.33817 0.33877 0.11878 0.11878 0.11878 0.01878 0.01878 0.01878	5.14597 4.00715 2.42206 1.44032 0.90811 0.459139 0.27722 0.21061 0.14833
5.55653 2.36528 1.39521 1.06891 0.49971 0.40971 0.10796 0.05129	6.15536 5.145536 1.95436 1.95468 1.95688 1.05130 0.75451 0.39633 0.18286 0.18286 0.18286 0.053991 0.053991 0.053991 0.053991 0.053991 0.053991	5.1468 4.15827 2.8719 8 1.50268 0.93838 0.67324 0.50493 0.2852 0.28720 0.28720
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5.92027 1.42220 1.71867 1.12948 0.43924 0.1871 0.11964 0.05291	6.29349 9.23349 9.23349 1.08444 0.81388 0.681388 0.233662 0.33666 0.33666 0.233666 0.09922 0.09922 0.09922 0.09922 0.09934	765 -194 -025 -584 -584 -584 -581 -191 -191
6.73626 3.7550 1.77550 1.77579 1.12968 5.90302 0.18916 0.05968	13.91037 5.27666 2.281966 2.281966 1.37733 0.51368 0.52166 0.34725 0.27713 0.17446 0.17446 0.17446 0.17446 0.17446 0.17446 0.17446 0.17446 0.17446 0.17446	8-77997 4-195704 1-87835 1-01762 0-5544 0-5544 0-25302 0-26302 0-26302 0-26302
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14.14206 3.572.6 1.67199 1.21057 0.90375 0.489375 0.13520 0.07557	25.29985 6.23568 3.5568J 2.46151 1.46151 1.46151 0.56076 0.26076 0.27914 0.27914 0.13657 0.13659 0.10659 0.10659 0.06261	16.27904 4.55033 3.13056 2.12917 1.14848 0.81395 0.6279 0.3184 0.3184 0.2018
14,49511 3-61499 1,96828 1,95731 1,00000 -5176 0,24198 0,07786	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
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APPENDIX A

0-10897 0-10897 0-09901 0-09901 0-09960 0-09960 0-019960 0-019960	6.00009 4.21052 2.21041 2.21053 2.21041 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317 0.35317	4 .5 8 1 4 9 8 .5 8 1 4 9 8 .5 8 1 4 9 8 2 3 3 9 8 2 8 2 8 2 8 2 8 2 8 2 8 2 8 2 8 2 8
0.12522 0.10959 0.09991 0.09995 0.09962 0.09695 0.03564 0.0336 0.01378 0.01378	6-40990 6-40687 6-89476 6-83537 0-89445 0-89445 0-89446 0-89445 0-89466 0-89466 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686 0-00686	4.58 230 3.50411 2.15463 0.42262 0.42262 0.18112 0.18112 0.08656 0.08656 0.08656 0.08656 0.09528 0.09528 0.09528
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0.13777 0.11272 0.09083 0.09083 0.09083 0.09983 0.09988 0.0398 0.02906 0.02906	7.25988 4.58108 3.01846 1.06541 0.28258 0.21594 0.12774 0.11774 0.11055 0.07210 0.04975 0.04695 0.00957	4.77345 6.00976 2.15638 0.48689 0.31999 0.18116 0.18116 0.18129 0.1823 0.08523 0.08523 0.01560 0.01596 0.01596
0.13861 0.11881 0.10020 0.09109 0.07596 0.04258 0.04258 0.03532 0.03636 0.01753	8.45170 3.04679 3.06145 1.39388 0.38435 0.28701 0.28703 0.12497 0.11480 0.12497 0.12497 0.12497 0.07244 0.05047 0.0504105	7.81686 4.04254 2.55692 0.50111 0.32386 0.14693 0.14693 0.097246 0.097246 0.097246 0.097246 0.097246
0.14257 0.11896 0.10020 0.003992 0.07394 0.04884 0.03633 0.03692 0.01878 0.01878	12.38450 5.08813 3.21826 1.44886 0.40181 0.40181 0.18737 0.18737 0.18737 0.05071 0.05071 0.06326 0.06326	6.45245 6.04510 2.69329 0.10744 0.350395 0.18865 0.18075 0.1820 0.008895 0.008895 0.008895 0.008895
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0.14403 0.12522 0.10695 0.09505 0.0866 0.03762 0.03762 0.03762 0.03762 0.03762	24.39590 5.46283 3.41641 1.55464 0.117996 0.233996 0.23258 0.23256 0.13225 0.10524 0.05433 0.05433 0.05403	15.69740 4.5786: 2.69547 1.2077: 0.356219 0.35621 0.13868 0.13868 0.13866 0.10667 0.09056 0.00086 0.03246 0.03246 0.0319
C.106633 C.10683 C.10683 C.1	48.06470 5.76283 3.50318 1.91360 0.62705 0.13283 0.132643 0.132663 0.132662 0.13204 0.13204 0.13204 0.13204 0.13204 0.13204 0.13204	36-1876 4-57866 3-01873 1-38886 (-868199 -1932 (-1936 (-1936 (-1946) (-1943) (-1943) (-1943) (-1943) (-1943) (-1943) (-1943) (-1943)
0.126603 0.126603 0.126660 0.049573 0.05660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660 0.039660	47.14079 5.97872 4.04474 5.8580 0.38644 0.38644 0.13394 0.12074 0.06037 0.064784 0.064784	4.58149 3.50128 3.50128 3.50128 3.50128 3.37733 0.25569 0.11656 0.11656 0.11656 0.11656 0.11656 0.11656 0.11656 0.11656 0.11656 0.11656

1.49756 0.78585 0.56069 0.40177 0.09530	1.31467 0.65336 0.44547 0.28538 0.09531 0.02451	13.04413 7.80163 4.94546 2.44652 1.628312 0.346810 0.25511 0.25511	10.36362 5.75085 3.94805 2.18504 1.43117 0.8048 0.38897 0.38897 0.13422 0.013422
1.51026 0.81685 0.59521 0.43357 0.03335	1.49769 0.70441 0.46952 0.40952 0.11916	13,15096 7,91273 4,96919 2,65255 1,75420 1,05091 0,61796 0,6110 0,27331 0,15825 0,09938	10.44850 7.33419 4.59696 2.49674 1.56046 0.35697 0.35699 0.35699 0.35699
1.81793 0.82234 0.6093 0.43353 0.18878 0.04065	1.700%5 0.70800 /.47662 0.30%%4 0.12%35	15.48913 8.40728 5.68727 2.70200 1.70200 1.68662 0.37334 0.10560	10.45512 7.47006 4.599874 2.49674 1.86268 0.80498 0.2924 0.2924 0.2924 0.29367 0.14515
2.04213 0.88492 0.63545 0.45308 0.22463	1,72238 0,76289 1,48442 0,33806 0,15660	15.52672 9.11125 5.74933 3.20424 1.14983 0.74182 0.74182 0.2818 0.28786 0.21265 0.05687	10.45696 1.47474 4.60066 2.53620 1.67792 0.38896 0.36805 0.29610 0.29610 0.1880
2.14077 0.88492 0.1456 0.24811 0.04878	1.87810 0.81692 0.850487 0.34044 0.03875	18-56728 9-56728 5-46182 3-46182 1-85455 1-85455 0-89491 0-59459 0-29428 0-11181 0-6011181	12.33765 7.47610 4.66140 2.546140 1.67792 1.11039 0.38187 0.29649 0.29649 0.08683
2.16786 1.00324 1.70794 0.46067 0.2481 0.04878	2.04231 0.86500 0.55977 0.3448 0.22465 0.03875	21.84456 6.83788 6.83764 3.60266 1.87239 1.87239 0.80491 0.29564 0.22646 0.22646	21.94651 4.86233 4.86233 2.65279 1.72495 1.14997 0.34549 0.24549
2.98081 1.08913 C.75513 C.33803 C.05310	2.31502 6.88500 6.60283 0.32448 0.22810 6.04306 0.01566	40.56848 10.45419 7.25419 2.74478 2.02842 0.52641 0.52641 0.52641 0.53403 0.12423 0.06241	39.79886 8.5119 5.30652 2.86233 1.179453 1.17055 0.96431 0.31209 0.24967 0.15607
3,19933 1,11602 0,78105 0,36138 0,05420 0,12451	2,36827 0,95325 0,62366 0,36601 0,24831 0,05310	63.05457 11.86463 7.28900 4.4818 2.11191 0.86961 0.86961 0.34067 0.34067 0.34600	40.57208 9.76854 3.42856 3.42856 1.2747 1.2.747 0.400.5 0.402.5 0.40372
3.66776 1.15721 1.78282 6.53938 6.37756 6.08522	3.19962 1.8923 0.62436 0.25359 0.05042	124,22978 12,29514 7,33353 4,59353 6,59384 7,56033 0,49384 7,56033 0,44509 0,213	96.70116 9.74472 5.74472 5.74620 2.02860 1.28311 0.78037 0.34545 0.34545 0.34545 0.25662
4.35654 1.31455 1.78456 0.55552 0.09277 2491	4.35693 1.15731 0.63223 0.64136 0.28597 0.02043	80.30542 12.75575 7.47412 4.68098 6.986098 1.61499 1.03855 0.45985 0.31207 0.31207 0.14043 0.09050	240.04161 9.77664 5.74984 5.74984 2.14675 1.29519 0.78951 0.3897 0.3897

APPENDIX .	Į	١	ı
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0.03590	29.70:14 9.14930 5.68452 5.88474 1.01346 0.71056 0.47117 0.24497	23.79097 7.10753 4.8810 1.56591 0.76659 0.56860 0.33711 0.18835	1 - 74 50 3 0 - 60 494 0 - 21 20 2 0 - 02 74 5	1.47 80 0.53353 0.13382 0.01745
0.04369	29.9441 10.61525 6.15238 2.87167 1.04661 0.71056 0.52260 0.26278	23.80403 7.21554 5.14979 2.28155 0.81155 0.95591 0.09591	0.03469 0.031609 0.031609 0.034609 0.034609	1.54464 0.60500 0.13382 0.02760
0.04681	35.35651. 11.01901 6.48177 2.94884 1.06585 0.71056 0.25946 0.14143	23.81025 8.17386 5.15385 2.85532 0.83954 0.25538 0.20538	1,000,5 0,4152 0,32418 0.9537	1.61620 0.62607 0.24437 0.03128
0-04682	37.72325 11.26068 6.53246 3.55242 1.06585 0.72136 0.53292 0.27691	28.09250 8.52754 5.15396 2.94911 0.53968 0.22001 0.11237	6.04168	1.74518 0.66899 0.24728 0.03312
0.04682	49.73953 11:43181 6.69837 4.12208 1.08204 1.72136 0.55382 0.14211	49.74396 3.73465 5.68502 3.55314 0.67622 0.44001 0.11237	2.54715 0.75618 0.38716 0.04537	1 - 27 6 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.04935	92.37343 12.94978 8.16558 4.2275 1.13147 0.73545 0.56803 0.16891	90.62103 6.76019 5.776019 3.62058 1.06594 0.71063 0.4869 0.22764 0.14213	5,733F6 C,93866 0,59177 C,04631	2.02372 0.75625 0.29093 0.04537
5 6 6 70 ° 0	143,57362 13,88148 8,20317 4,80876 1,13147 0,3825 0,30975	00 00 00 00 00 00 00 00 00 00 00 00 00	3,13416 0.988.05 0.39985 0.07928	2.73412 0.76765 0.29436 0.65004
0.06242	282.56792 17.76411 8.42630 4.81376 1.29498 0.295928 0.295528	22697K605 11.3427 11.3427 10.341 10.3	3.25581 6.99508 6.99508 6.09143	3.2541) C.81456 U.91246 C.08144
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BUANTITIES A THREUCH J AND L THRUGGH Z JRDERED BY MACNITUDE

SILICON DEVICES CHLY FOR L. M. AND N

FOR VALUES OF A THROUGH 3 AND L THROUGH 2 LESS THAN IN VALUE TABULATED IS INVERSE OF THE VALUE LESS THAN I

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211-31424	11011	99.01933	17.30.110	27.000	16001-04	06674-14	34.52158	25.09119	713517	18.84529	15.54127	12.78578	11.42139	0.50023	7.39740	5.23.3	4.56856	4.01265	2.67840	2.38080	1.74797	1.54621	1.31511	1.00508		222 -29 97		-						46.03 74					22.11 60		17.59 55				_	•
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7-94 34 36 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	65744 64707 64707 64707 64707 135584 135584 135587 135587 17538 17	63.52 77.22 63.52 77.22 63.54 65.6 25.74 61.7 27.75 60.0 18.77 50.0 18.77 50.0 18.77 50.0 17.99 66.0 9.10 36.6 6.03 26.6 7.67 36.6 7.67 36.6 7.67 36.6 7.67 36.6
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2-19 12-2 1-71 8-3 1-4 6-4 1-08 0-6	82.48915 36.99565 14.72655 2.965640 2.96712 1.95186 1.34759 41.92 84.1 41.92 84.1 41.92 84.1 41.92 84.1 25.15 73.9 14.72 63.8 4.30 43.3 2.96 33.3 2.96 33.3 1.52 13.6 1.52 13.6	37725 45 E 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	31.66.7 86.46 18.66.3 76.10 11.66.3 76.10 11.56.3 76.50 11.56.3 85.2 11.56.3 85.2
2.79 16.7 2.21 12.8 1.78 8.9 1.42 5.0 1.21 1.1	85.54433 32.99565 17.59767 2.99585 2.99581 2.99581 1.38886 1.38840 1.38886 1.38886 1.38886 1.38886 1.38886 1.38886 1.38886 1.38886 1.38886 1.38886 2.9734.8 2.9734.8 2.9734.8 2.9734.8 1.38886	82-6729 36-91898 25-56302 17-59209 10-51517 5-2763 4-27916 3-32512 2-46359 1-76035 1-54514 1-25109	56-56 81.1 15-56-56 81.1 10-17 70.8 10-17 65.9 7-66 60.6 6-67 56.0 6-67 56.0 6-73 66.7 6-73 66.7 6-73 66.7 6-73 66.7
17.2 13.3 9.4 1.7	158.40302 33.53993 18.46035 6.03440 3.03070 2.12019 1.41433 1.	143 - 935 34 41 - 1804 26 - 388 14 17 - 629 61 10 - 555 26 7 - 623 86 4 - 328 88 5 - 683 79 5 - 683 79 7 - 640 91 1 - 642 15 1 -	200 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
2 - 2 - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3 -	343 -02193 -02193 -02193 -0219	216-25616 47.36977 28-64044 13-62692 12-27025 7-85938 5-92122 4-3985 1-59838 1-54179 1-6426 1	
3-16 17-8 2-46 13-9 2-60 10-0 1-53 6-1 1-31 2-2	791-89551 41-92491 21-12/39 38-38498 38-38498 2-35828 1-48553 791-90 98-6 57-17 88-4 39-7-17 88-4 57-17 88-4 39-7-17 88-4 10-06 58-1 5-C1 47-8 1-45 27-5 1-45 27-5 1-39 7-2		20.14 03.3 210.9 70.3 210.9 70.3 10.79 72.7 7.95 67.4 7.95 67.4 6.62 56.8 6.45 56.8 6.45 56.8

APPENDIX A				

	44.76213 9.88497 7.26999 4.04855 1.69942 1.17537	20.09686 6.61688 2.32209 1.34763	164.41762
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2.73 31.8 2.17 26.5 1.76 21.2 1.65 15.9 1.64 10.6 1.17 5.3	55.49240 21.244240 10.98830 6.34112 6.83285 3.632499 1.93043 1.93043 1.932499 7.03 52.9 7.03 52.9	24.1064 9.17362 2.00421 1.55083 27.57 86.7 17.97 71.1 6.62 55.6 3.22 40.0 1.77 24.4	169.22473
6 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	26-31712 13-94043 3-94043 3-22408 1-61716 13-3 73-3 57-8 42-2 56-7	172.94226 121.94649
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